

# Surface metrology and polishing techniques for current and future-generation EUVL optics

**Regina Soufli**

*regina.soufli@llnl.gov*

**Lawrence Livermore National Laboratory**

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## Contributors

- *Lawrence Livermore National Lab:*  
Sherry L. Baker, Jeff C. Robinson, Eberhard Spiller,  
Mónica Fernández-Perea, Tom McCarville, Michael Pivovarovff
- *Lawrence Berkeley National Lab:* Eric M. Gullikson
- *Hyperion Development :* Russell Hudyma
- *SLAC National Accelerator Lab:*  
Peter Stefan, Sebastien Boutet, Paul Montanez
- *Lockheed Martin Corporation:* Dennis Martinez-Galarce
- Other contributors will also be acknowledged throughout this presentation



# Outline

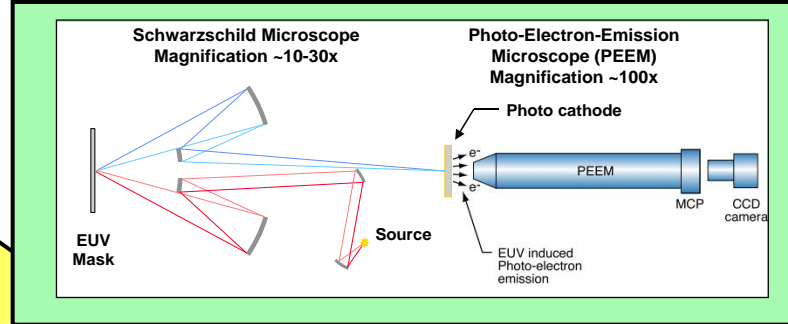


- Overview of diffraction-limited EUVL systems
  - Metrology capabilities at LLNL and LBNL
  - EUVL projection optics: figure, MSFR and HSFR results and implications
  - Zerodur vs. ULE as substrate materials for next-generation EUVL projection optics
  - Si, SiC and other composite ceramics as candidate substrate materials for EUVL collector optics
  - Novel smoothing technologies for EUVL collector substrates
  - Recent advances in optic fabrication technologies for EUV solar physics and x-ray FELs and their relevance to EUVL optics
  - Perspectives on 6.x nm lithography
  - Summary and conclusions
- 
- ***Unless otherwise indicated, all surface metrology results and analysis in this presentation were produced at LLNL***
  - ***Any results or references to commercial vendors in this presentation do not by any means imply endorsement of these vendors or their products***

# EUVL systems have greatly evolved in complexity over the past 15 years



**10x1 - 1996**  
**10x2 - 1999**  
**0.1 NA**  
**“Microstepper”**

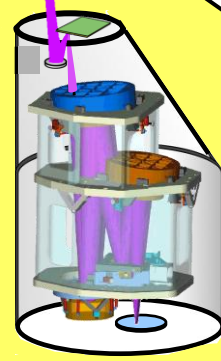


**EUV AIMS Tool**  
**Proposed 2001**

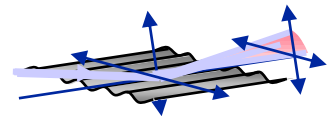
**ETS POB1 - 2000**  
**0.1 NA**  
**Full-field scanner**



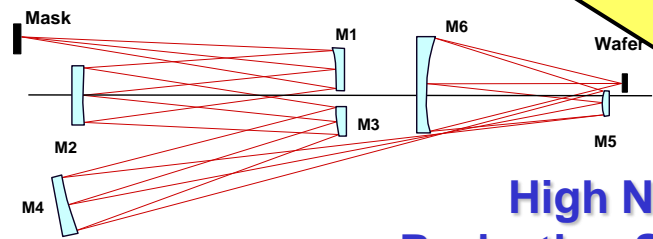
**SES POB2 - 2001**  
**0.1 NA**  
**Static field**



**MET**  
**2002-today**  
**0.3 NA**  
**μstepper**



**Ripple-Plate Condenser**



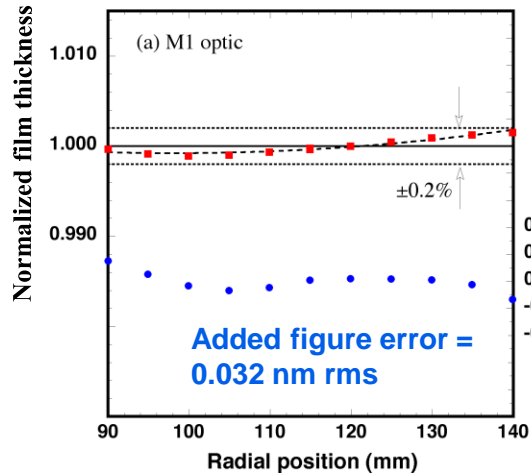
**High NA**  
**Projection System**



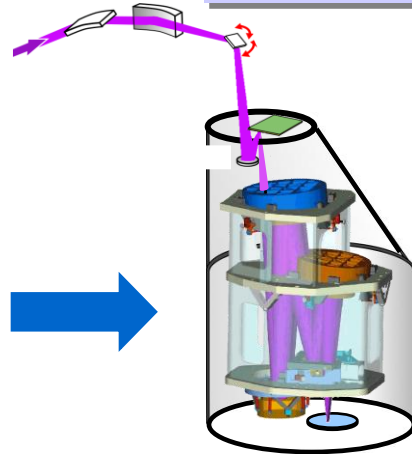
# ETS and MET projection optics demonstrated multilayer-added figure errors < 0.05 nm rms and sub-diffraction-limited performance



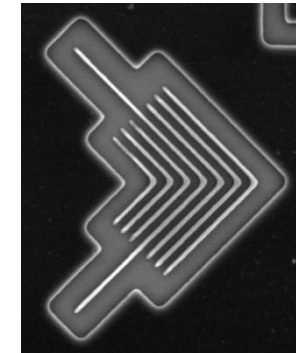
**M1 mirror, PO Box 2**



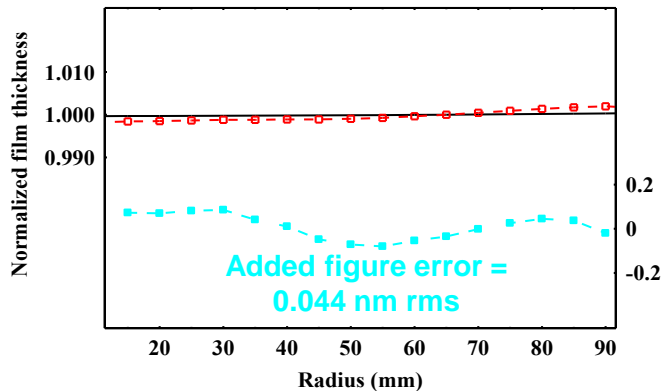
**SES at ALS**



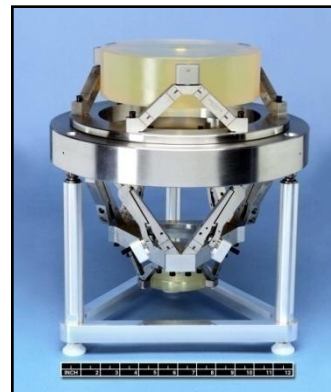
**39-nm, 3:1 elbows (Patrick Naulleau, LBNL)**



**M2 mirror, MET Set 1**



**MET camera**



**Measured wavefront = 0.55 nm rms**

K. A Goldberg et al, J. Vac. Sci. Technol. B 22(6), 2956-2961 (2005)

**Printed 25 nm equal-line, and 29 nm isolated-line features**

P. P. Naulleau et al, Proc. SPIE 5751, 56-63 (2005)



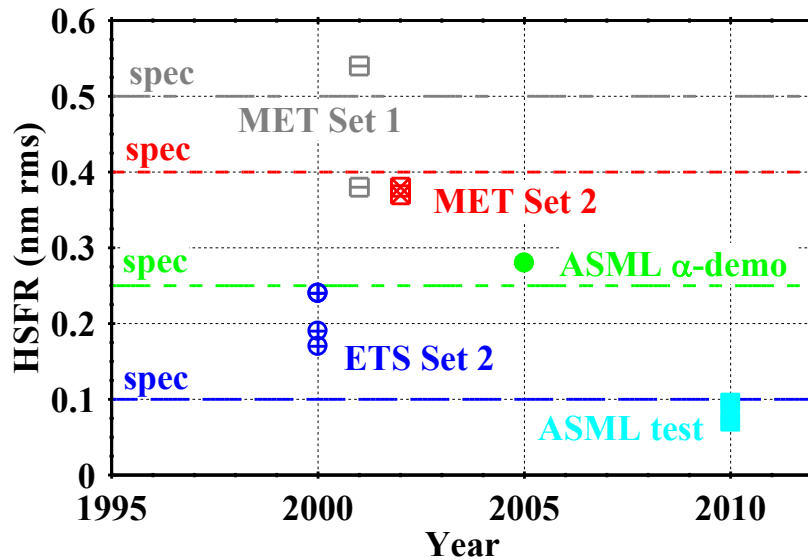
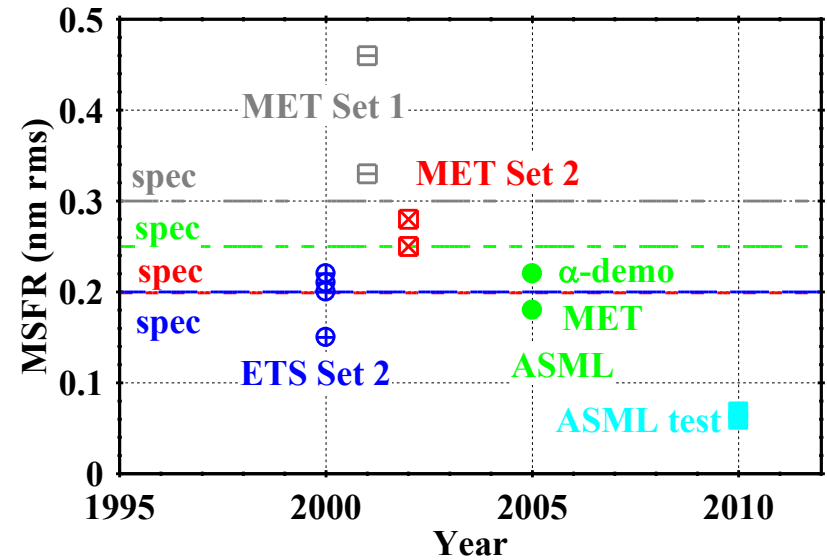
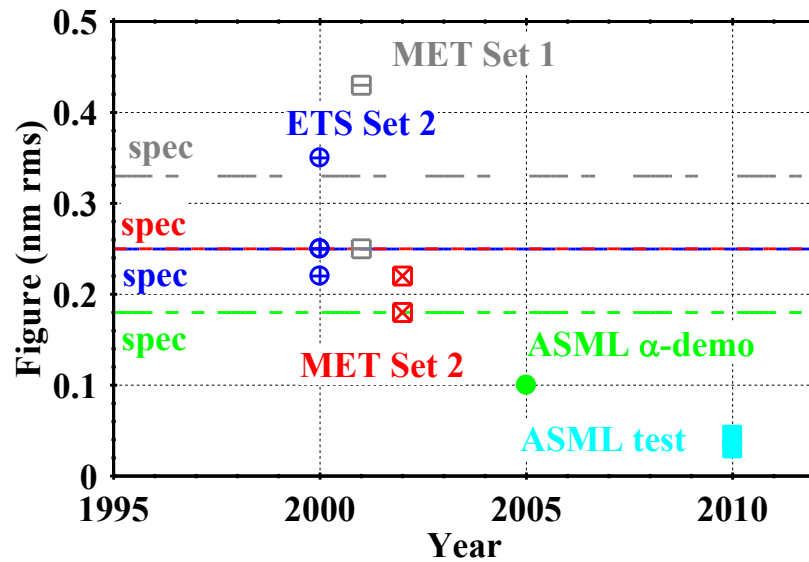
# EUVL optics: spatial frequency ranges and specifications

	Figure (rms)	MSFR (rms)	HSFR (rms)
<b>Projection- Microfield (MET)</b>	~0.1 nm	~0.1 nm	~0.1 nm
<b>Projection – Scanning (<math>\alpha</math> or production)</b>	~0.1 nm ( $\alpha$ ) < 0.1 nm (prod.)	~0.1 nm ( $\alpha$ ) < 0.1 nm (prod.)	~0.1 nm ( $\alpha$ ) < 0.1 nm (prod.)
<b>Collector</b>	~ $\mu$ rad	~0.1 nm	~0.1 nm

-  Critical
-  Important

**EUVL requires extremely challenging specifications for the figure, MSFR and HSFR to be simultaneously met on large-area optical surfaces**

# Historical evolution of figure, MSFR and HSFR of EUVL projection optics and comparison with specs

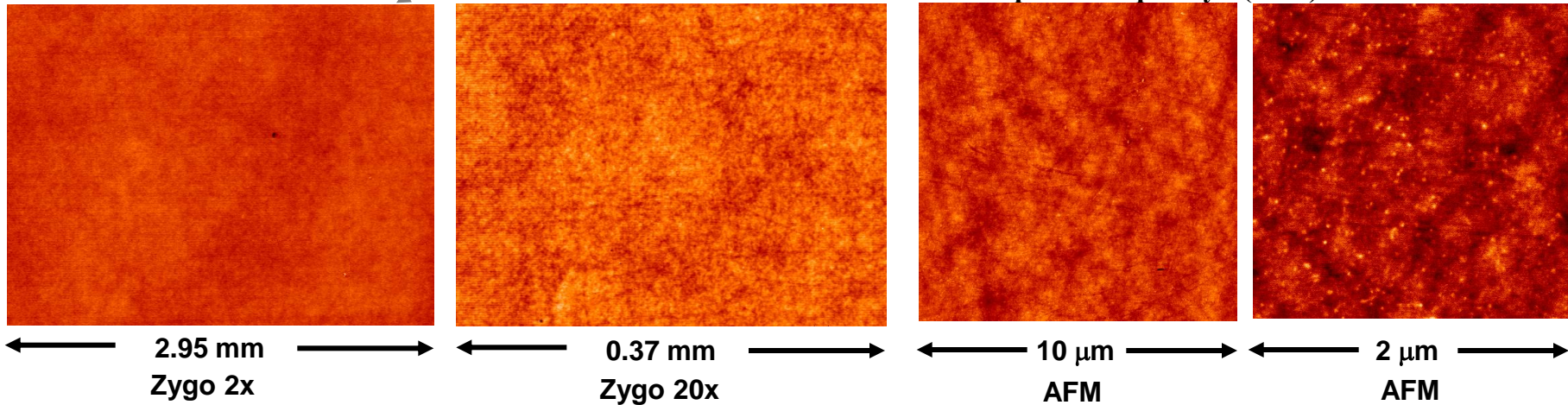
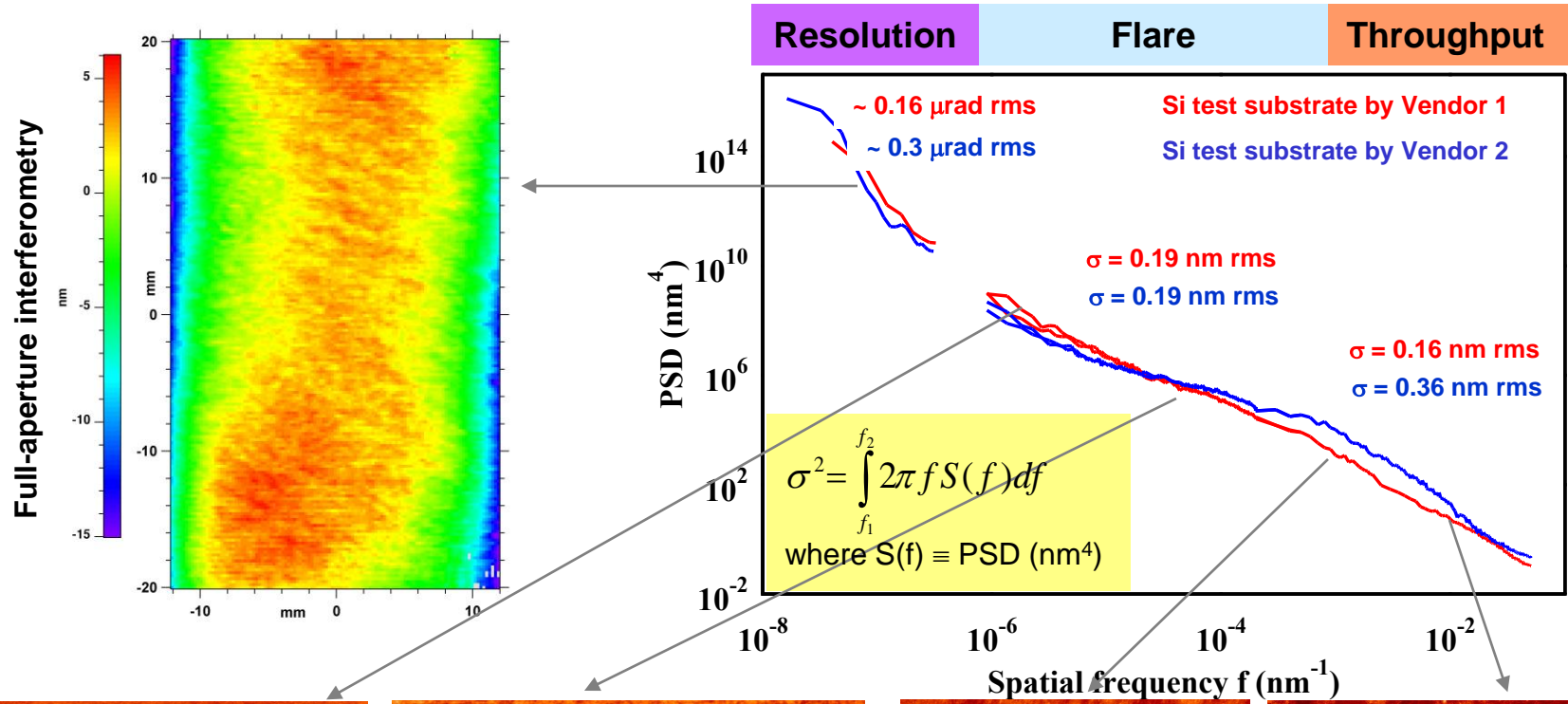


- Note that mirrors in plotted PO systems have different sizes, aspheric departures, etc
- Spatial frequency range of relevance for MSFR varies among plotted PO systems
- Nevertheless, a comparison among plotted results and specifications can reveal useful information on the evolution of polishing capabilities for EUVL projection optics

R.Soufli, et al, Proc. SPIE 4343, 51-59 (2001).  
 U. Dinger, et al, Proc. SPIE 5193, 18-28 (2004).  
 H. Meiling, et al, Proc. SPIE 5751 90-101 (2005).  
 R. Soufli, et al, Appl. Opt. 46, 3736-3746(2007).  
 M. Lowisch, et al, Proc. SPIE 7636, 763603 (2010).



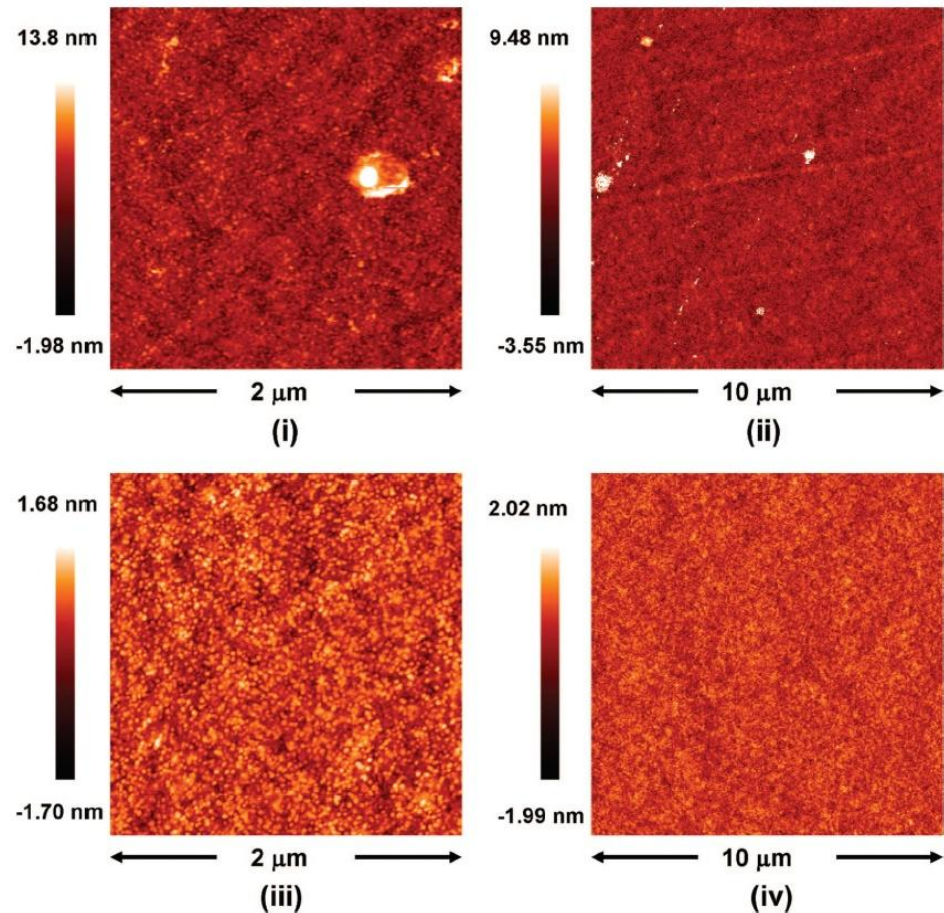
# EUVL mirrors require state-of-the-art metrology for the figure, MSFR and HSR



# LLNL cleaning facility for optical substrates removes microscopic contamination while maintaining surface finish



Custom-developed process includes: rinsing in a water-based solution, followed by drying in N<sub>2</sub> environment using semiconductor-grade system (*YieldUP*<sup>TM</sup>, pictured). Located next to multilayer deposition system.



LLNL AFM images on a Zerodur substrate: (i), (ii) as-received and (iii), (iv) after cleaning.

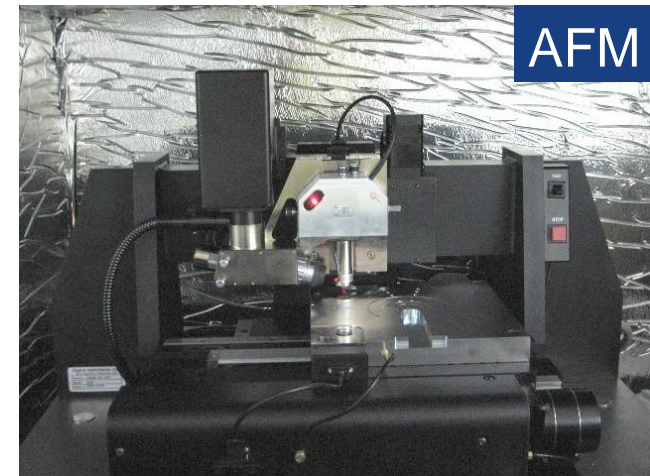
R. Soufli, S. L. Baker, *et. al*, Appl. Opt. 46, 3156-3163 (2007).





# LLNL precision surface metrology lab

- **Digital Instruments Dimension 5000™ Atomic Force Microscope (AFM)** includes acoustic hood and vibration isolation. *Noise level = 0.03 nm rms*
- **Zygo NewView™ Optical Profiling Microscope**
- **LEO 1560™ Scanning Electron Microscope (SEM)**
- **Full aperture interferometers (not shown)**

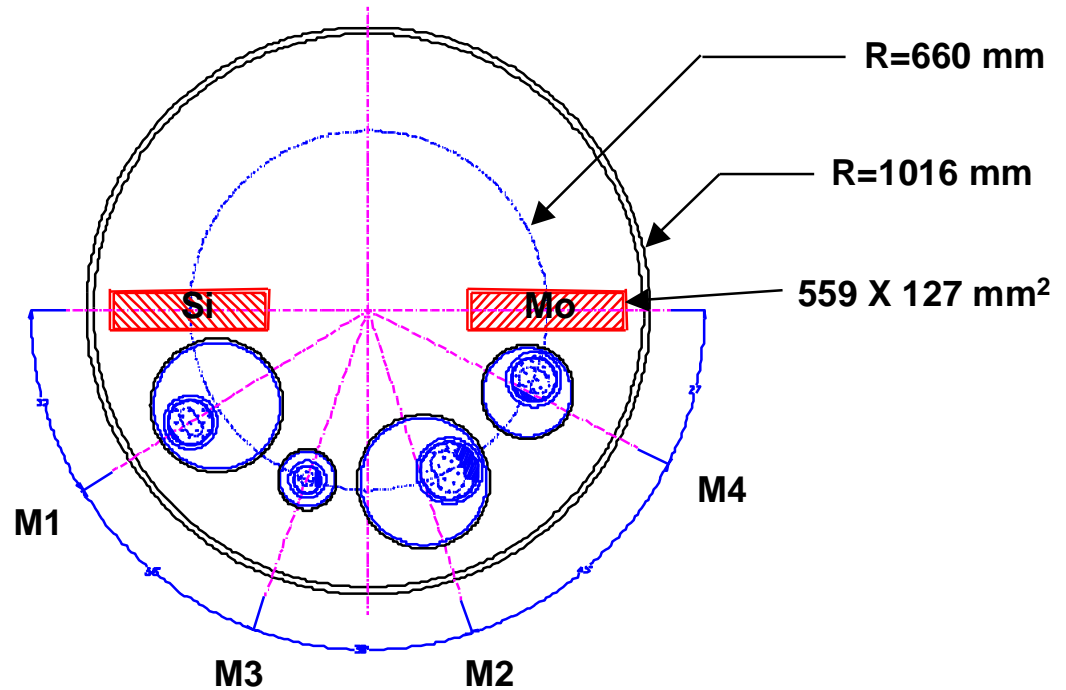




# DC-magnetron sputtering is a proven deposition technique for the multilayer-coating of EUVL camera and collector optics

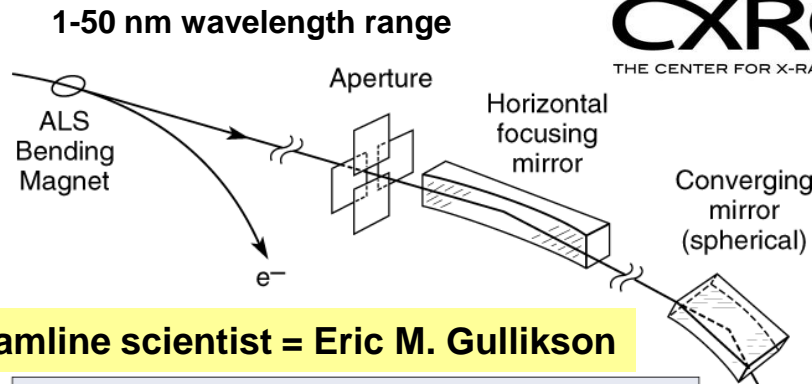


Underneath view of LLNL chamber lid with 5 sputtering targets



4-mirror and 2-mirror EUV cameras have been multilayer-coated in a single deposition run, achieving optic-to-optic wavelength matching within  $1\sigma = 0.010$  nm. Maximum optic size that can fit in chamber is 450 mm in diameter

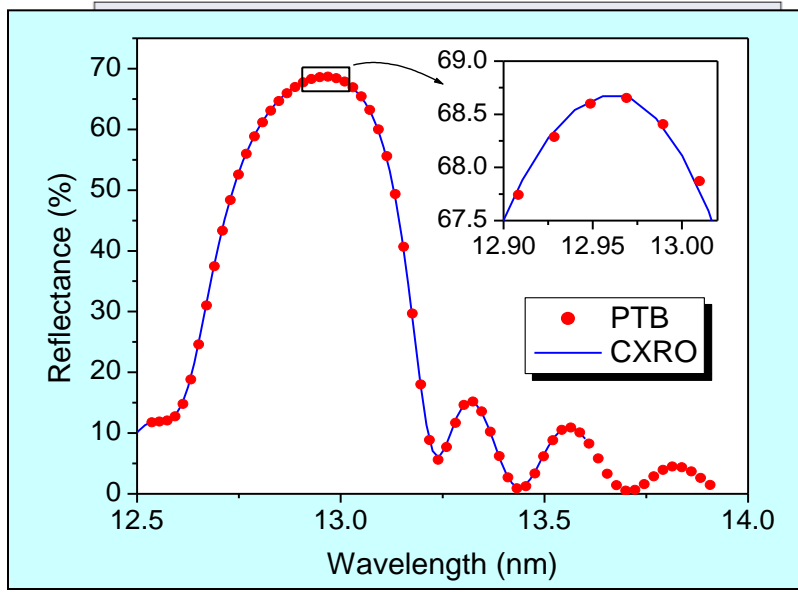
# CXRO's beamline 6.3.2. at the ALS synchrotron (LBNL) is the world reference standard for EUV/x-ray reflectance, scattering and transmission measurements



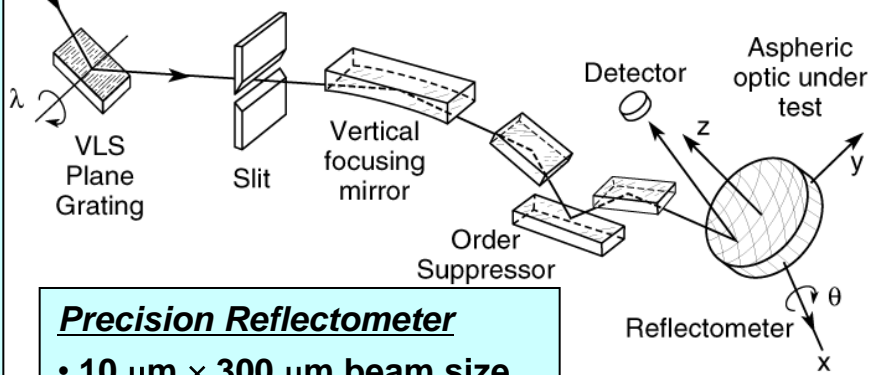
## Beamline Specifications

- Wavelength precision: 0.007%
- Wavelength uncertainty: 0.013%
- Reflectance precision: 0.08%
- Reflectance uncertainty: 0.08%
- Spectral purity: 99.98%
- Dynamic range:  $10^{10}$

Beamline scientist = Eric M. Gullikson



Cross-calibration results are shown between beamline 6.3.2 (CXRO) and PTB, BESSY synchrotron (Berlin, Germany)



## Precision Reflectometer

- 10  $\mu\text{m}$   $\times$  300  $\mu\text{m}$  beam size
- 10  $\mu\text{m}$  positioning precision
- Angular precision 0.01 deg
- 6 degrees of freedom
- Sample size up to 200 mm

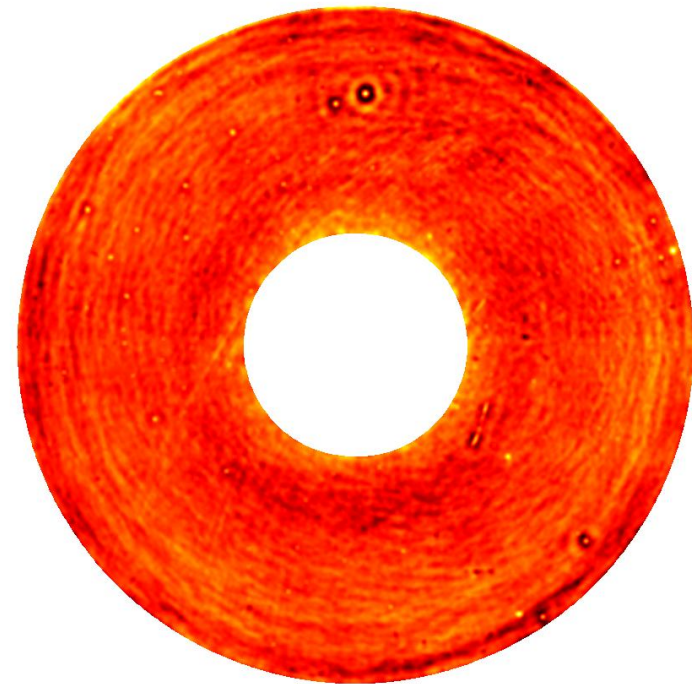
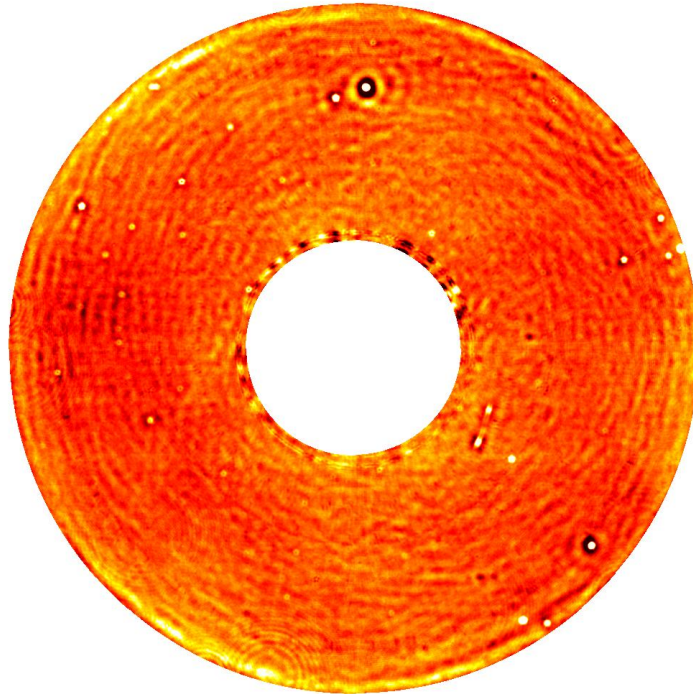
LG156

# Side-by-side comparison of the Zeiss and LLNL full-aperture interferometry for the MET primary substrate figure



**Zeiss interferometer**  
**Flipped and rotated to register**  
**0.22 nm rms when clipped and binned**

**LLNL Phase-shifting diffraction (PSDI) interferometer**  
**Magnification adjusted fractionally by  $1.7 \times 10^{-5}$**   
**0.29 nm rms when clipped and binned**



-1 nm



+1 nm

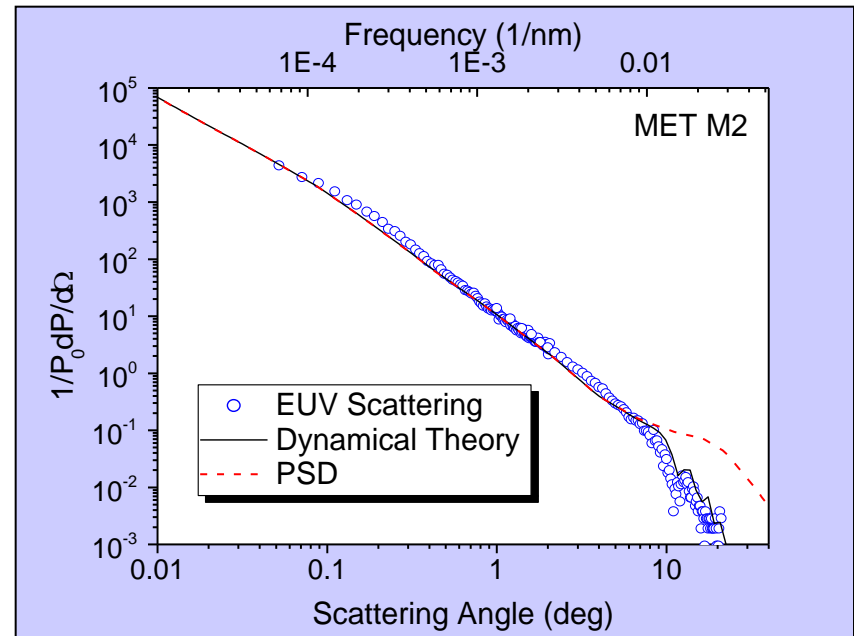
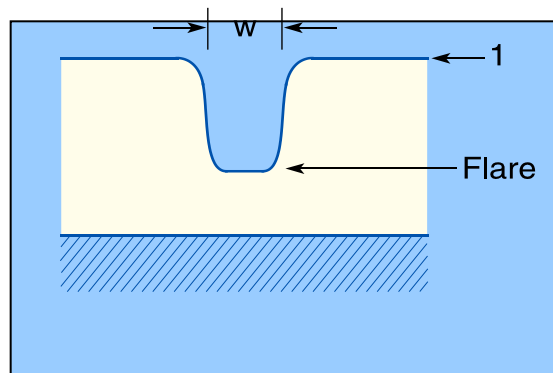
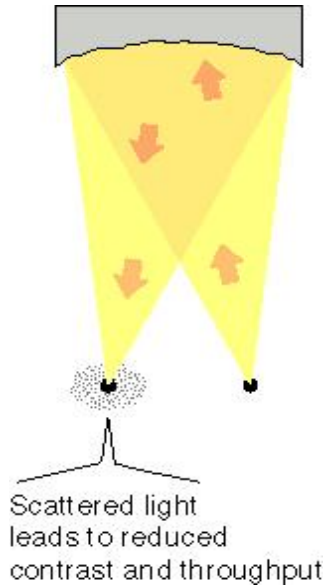
G. E. Sommargren, D. W. Phillion, M. A. Johnson, N. Q. Nguyen, A. Barty, F. J. Snell, D. R. Dillon, L. S. Bradsher, "100-picometer interferometry for EUVL", Proc. SPIE 4688 316-328 (2002).



# EUV optics are especially susceptible to roughness and scattering



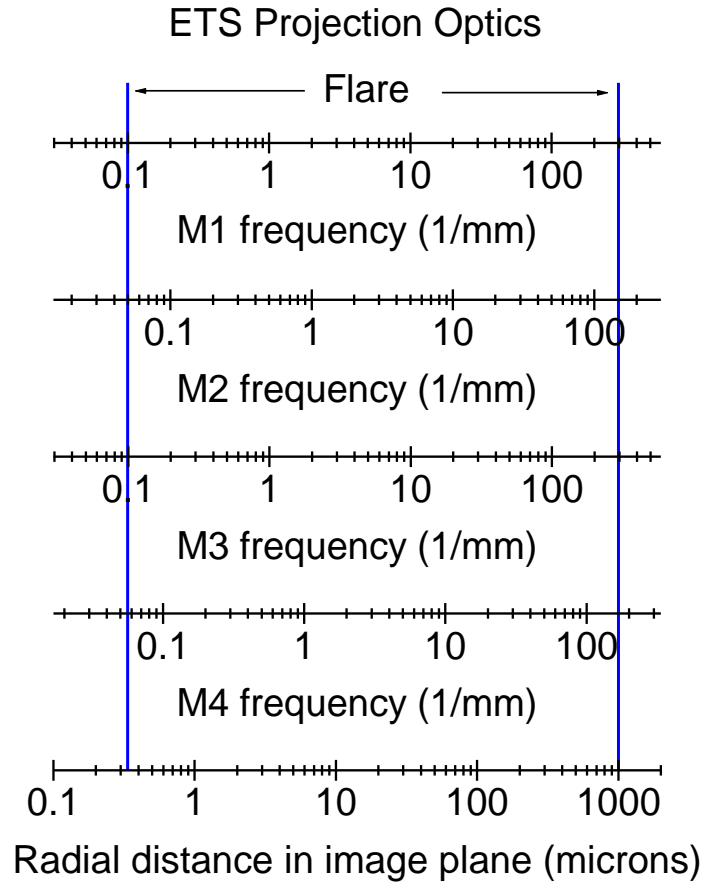
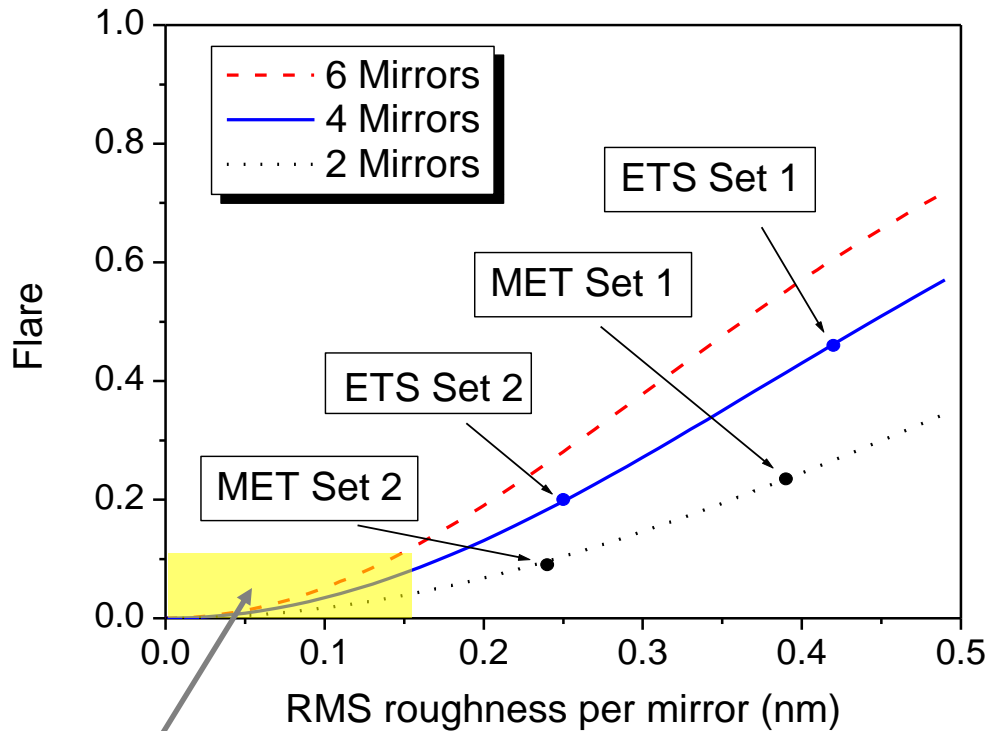
- As the wavelength  $\lambda$  is reduced, scattering increases with  $1/\lambda^2$ .
- Roughness of EUV optics must be controlled, otherwise scattering will result in loss of contrast or Flare.
- The scattering angular distribution has been measured and can be predicted from the surface roughness.



Courtesy E. M. Gullikson (LBNL)



# Improved MSFR leads to lower flare

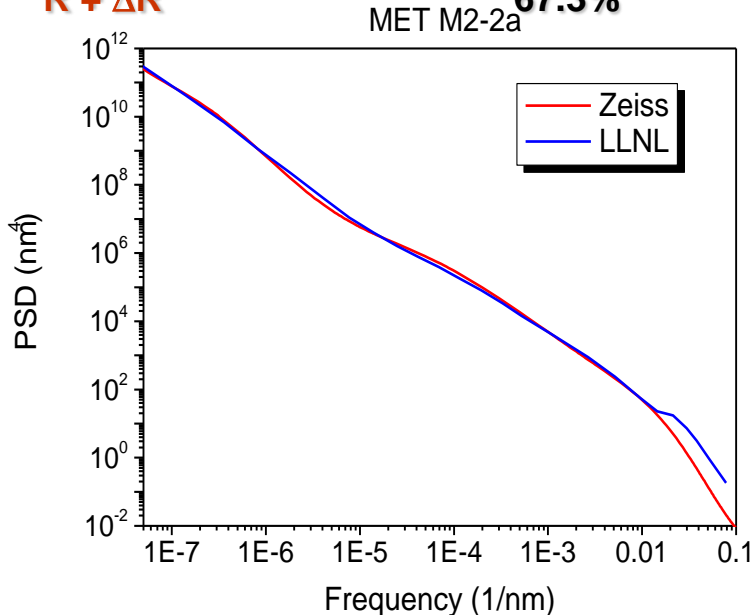


**< 10 % flare for a 6 or 8-mirror system requires MSFR < 0.15 nm rms**

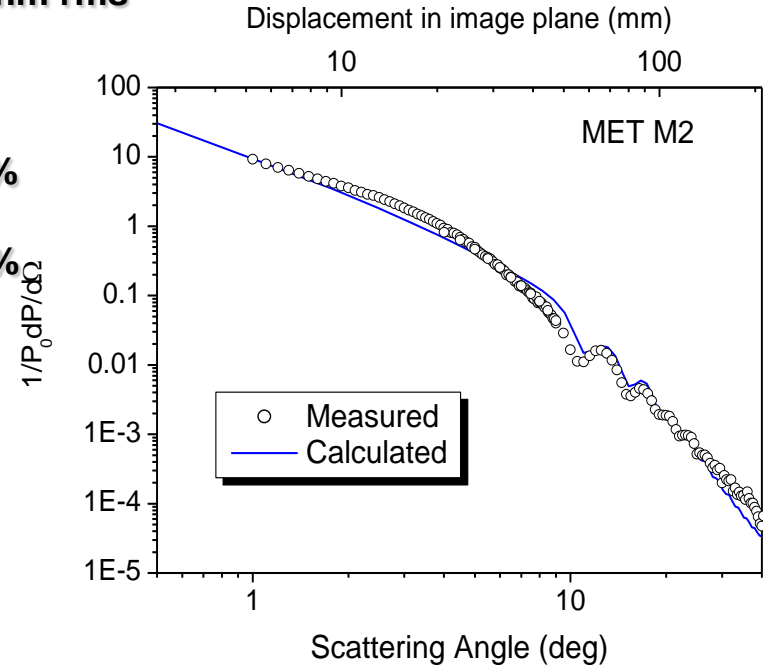


# Metrology cross-validation between different facilities and independent measurements and models

	MET 1 (primary)	MET 2 (secondary)
<b>Substrate HSFR</b>	<b>0.37 nm rms</b>	<b>0.32 nm rms</b>
<b>Expected loss <math>\Delta R</math></b>	<b>6.1%</b>	<b>5.2%</b>
<b>Measured R</b>	<b>61.2%</b>	<b>62.4%</b>
<b>R + <math>\Delta R</math></b>	<b>67.3%</b>	<b>67.6%</b>



**LLNL / Zeiss metrology validation**



**LLNL metrology / scattering model / ALS scattering measurements validation**

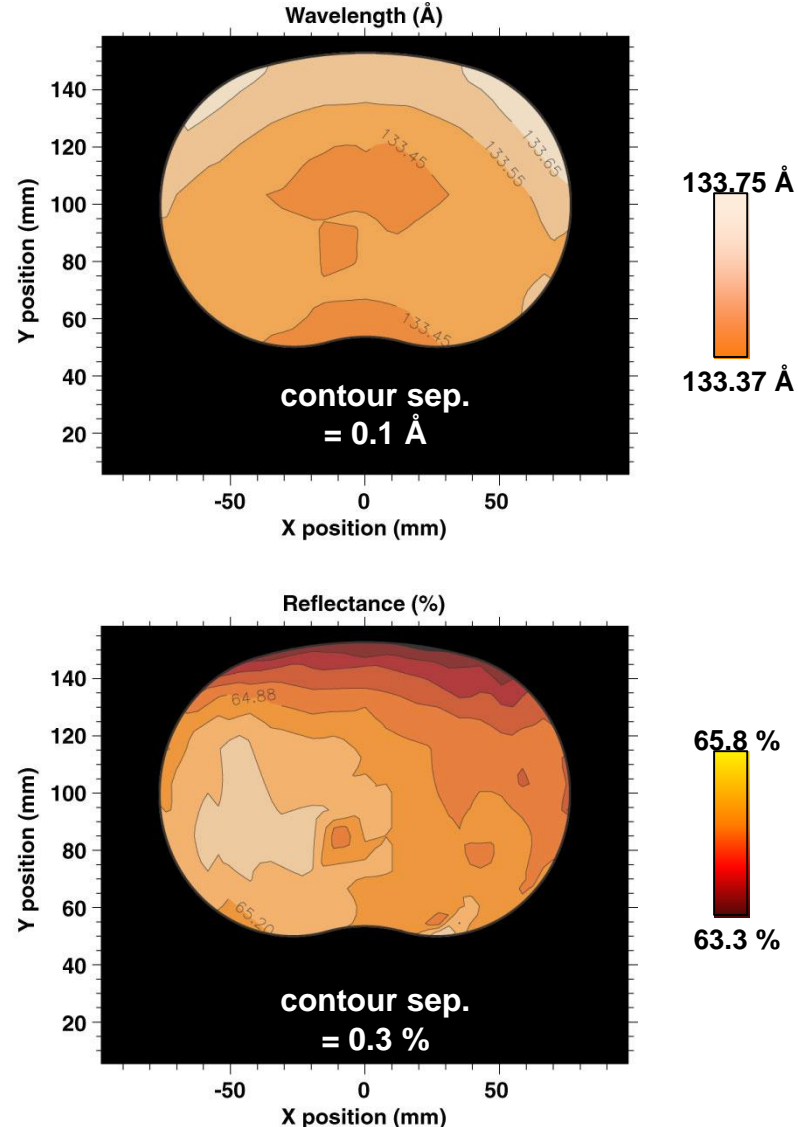
R. Soufli *et al.*, *Appl. Opt.* 46, 3736-3746 (2007)

D. G. Stearns, "Stochastic model for thin film growth and erosion," *Appl. Phys. Lett.* 62, 1745-7 (1993).

E. M. Gullikson, "Scattering from normal incidence EUV optics", *Proc. SPIE* 3331, 72-80 (1998).

D.G. Stearns *et al.*, "Non-specular x-ray scattering in a multilayer-coated imaging system", *J. App. Phys.* 84, 1003-1028 (1998).

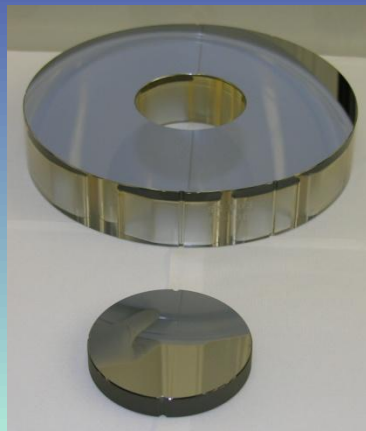
# Accurate EUV reflectance measurements provide an additional method to verify substrate HSPR uniformity



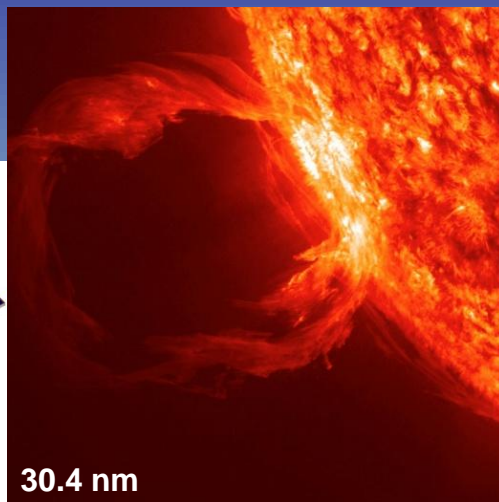
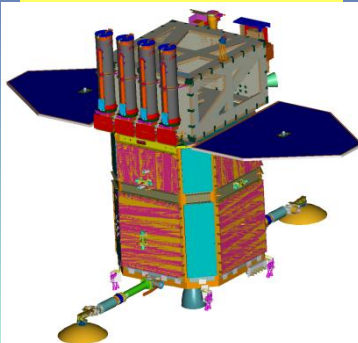
2D contour maps of ETS optic M2 obtained at ALS beamline 6.3.2



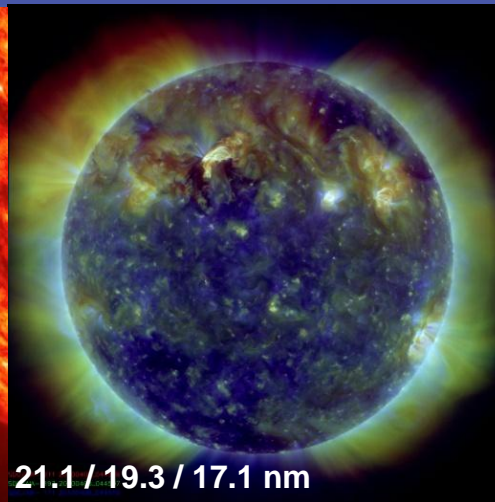
# We have developed EUV multilayer optics and precision metrologies for next-generation solar physics and space weather satellites



7 EUV wavelengths  
(9.4 nm to 33.5 nm)



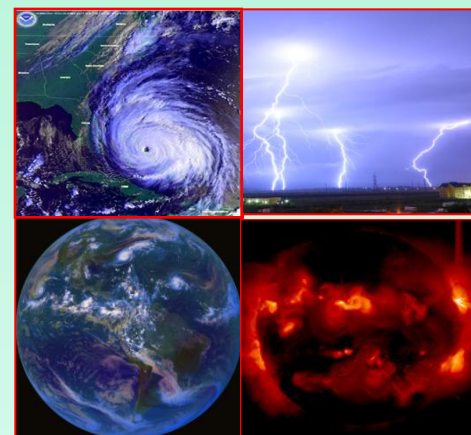
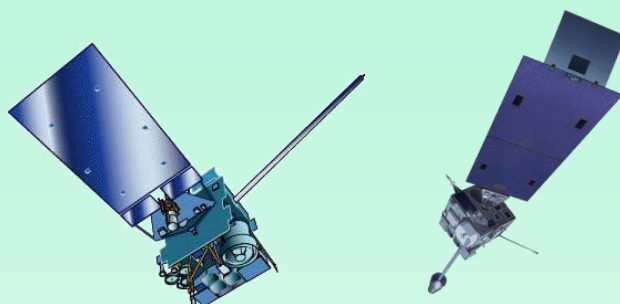
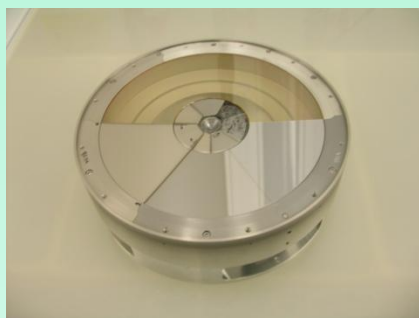
30.4 nm



21.1 / 19.3 / 17.1 nm

R. Soufli, *et al*, Proc. SPIE 5901, 59010M (2005).  
 R. Soufli, *et al*, Appl. Opt. 46, 3156-3163 (2007).  
 P. Boerner *et al*, Solar Physics (2011).  
 J. R. Lemen *et al*, Solar Physics (2011).

**NASA's Solar Dynamics Observatory (SDO). Launch date: February 11, 2010.**  
<http://sdo.gsfc.nasa.gov>



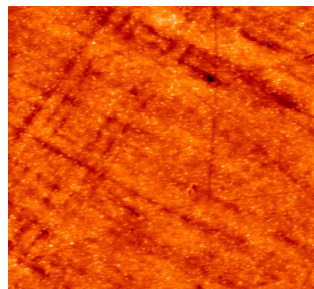
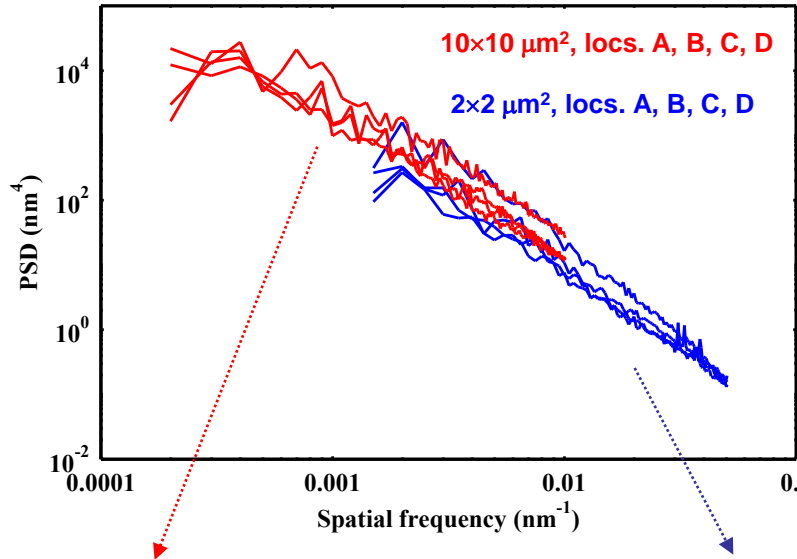
Multilayer-coated test mirrors for NASA/NOAA's GOES-R space weather satellite. 6 EUV wavelengths, 9.4 nm to 30.4 nm.  
 Launch date: 2014

# AFM measurements reveal surface morphology related to specific polishing techniques

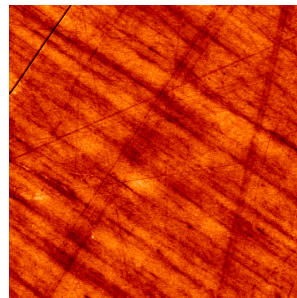


Atmospheric Imaging Assembly (AIA) instrument, Solar Dynamics Observatory (SDO)

Vendor 1, Zerodur substrate

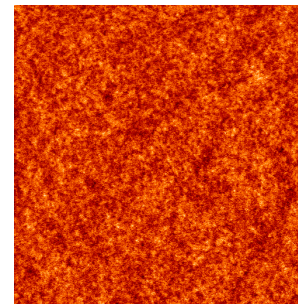
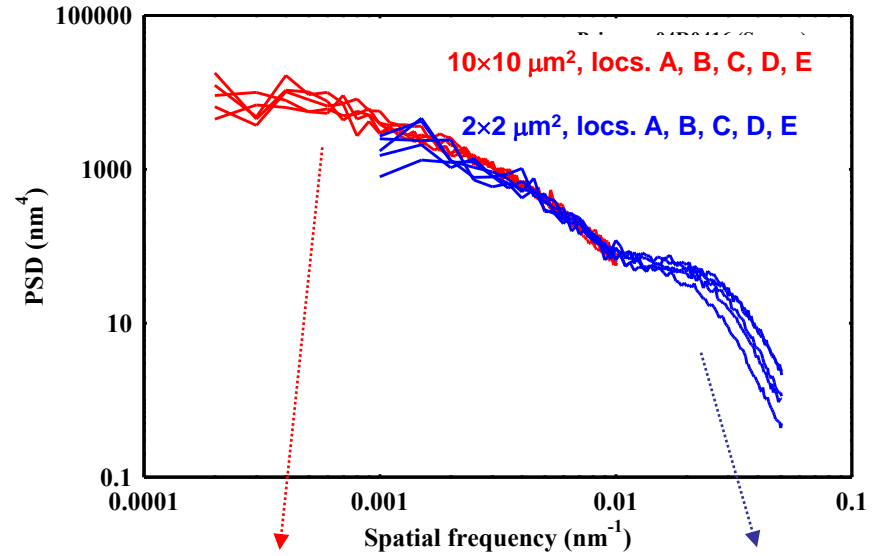


10x10 μm², loc. B

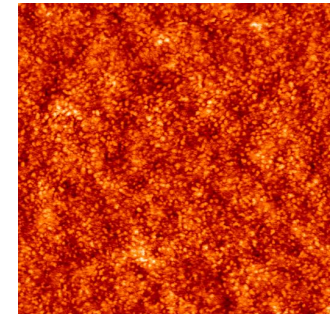


2x2 μm², loc. B  
 $\sigma = 0.14 \text{ nm rms}$

Vendor 2, Zerodur substrate



10x10 μm², loc. E



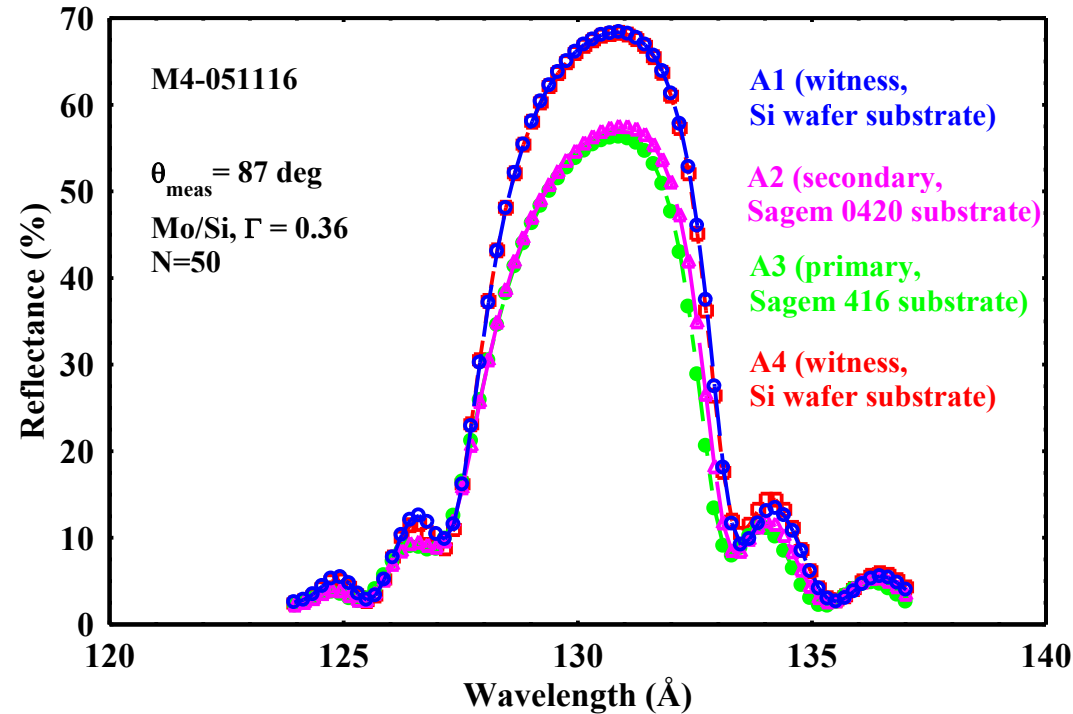
2x2 μm², loc. E  
 $\sigma = 0.51 \text{ nm rms}$

$$\sigma^2 = \int_{f_1}^{f_2} 2\pi f S(f) df \quad \text{where } S(f) \equiv \text{PSD (nm}^4\text{)},$$

$f_1 = 10^{-3} \text{ nm}^{-1}$ ,  $f_2 = 5 \times 10^{-2} \text{ nm}^{-1}$

R. Soufli, S. L. Baker, D. L. Windt, E. M. Gullikson, J. C. Robinson, W. A. Podgorski, L. Golub, Appl. Opt. 46, 3156-3163 (2007)

# EUV reflectance of multilayer-coated mirrors is consistent with substrate roughness measured by AFM



Flight mirror	Primary (Sagem 04R0416)	Secondary (Sagem 04R0420)
Substrate roughness (Å rms)	5.0	5.2
$R_{\text{peak}}$ (%)	56.2	58.8
$\Delta R^*$ (% absolute)	8.5	8.4
$R_{\text{peak}} + \Delta R$	64.7	67.2

\* $\Delta R$  = predicted reflectance loss due to high-spatial frequency roughness, based on AFM measurements of the substrate and on a multilayer growth model. Calculation performed by E. M. Gullikson, LBNL.

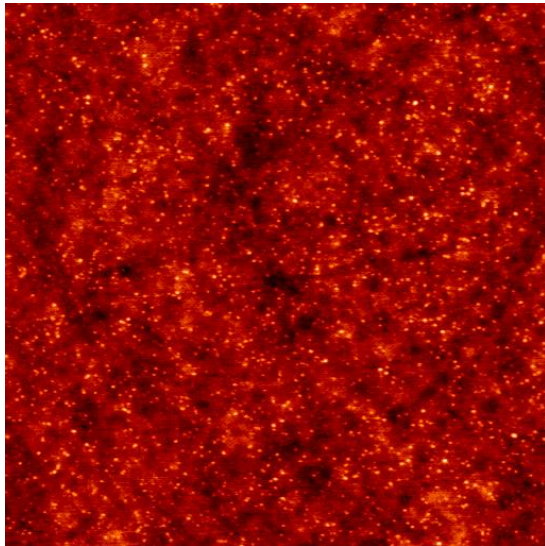




# Zerodur as substrate material for EUVL projection optics

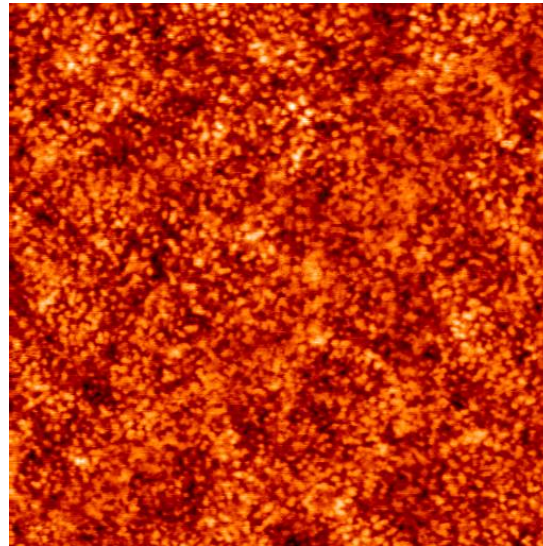
- Zerodur® (Schott) is an ultra-low-expansion glass ceramic
- 2-phase material: fused silica (amorphous) and quartz (crystalline).
- It has been used to make the most accurate projection/imaging optics for EUVL, EUV solar physics (TRACE, SDO, GOES-R, etc), x-ray astronomy (Chandra), and other applications
- Lowest achievable HSFR and MSFR may be ultimately limited due to dual phase of the material

Polished by computer controlled grinding/polishing



AFM  $2 \times 2 \mu\text{m}^2$ , HSFR = 0.14 nm rms

Polished by ion beam



AFM  $2 \times 2 \mu\text{m}^2$ , HSFR = 0.48 nm rms

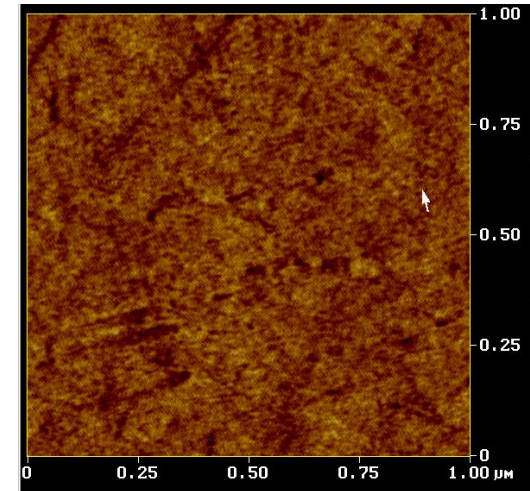
In both AFM images, lighter-color areas represent quartz crystallites protruding within amorphous silica

# ULE as candidate substrate material for EUVL projection optics



Courtesy: Chris Walton and  
Cindy Larson (LLNL)

- ULE® (Corning) is an ultra-low-expansion glass
- ULE = titania silicate =  $\text{SiO}_2$  (> 90%)+  $\text{TiO}_2$  (< 10%)
- It has been used to make super-polished mask blanks for EUVL, optics for astronomy (Hubble, Gemini) and other applications
- Striae and inhomogeneities have been preventing its use as substrate for EUVL projection optics



AFM  $1 \times 1 \mu\text{m}^2$ , HSFR = 0.16 nm rms. Obtained on ULE mask blank

HSFR = 0.06 nm rms has been measured on ULE at LLNL [P. Mirkarimi et al, Appl. Opt. 40, 62-70 (2001)].

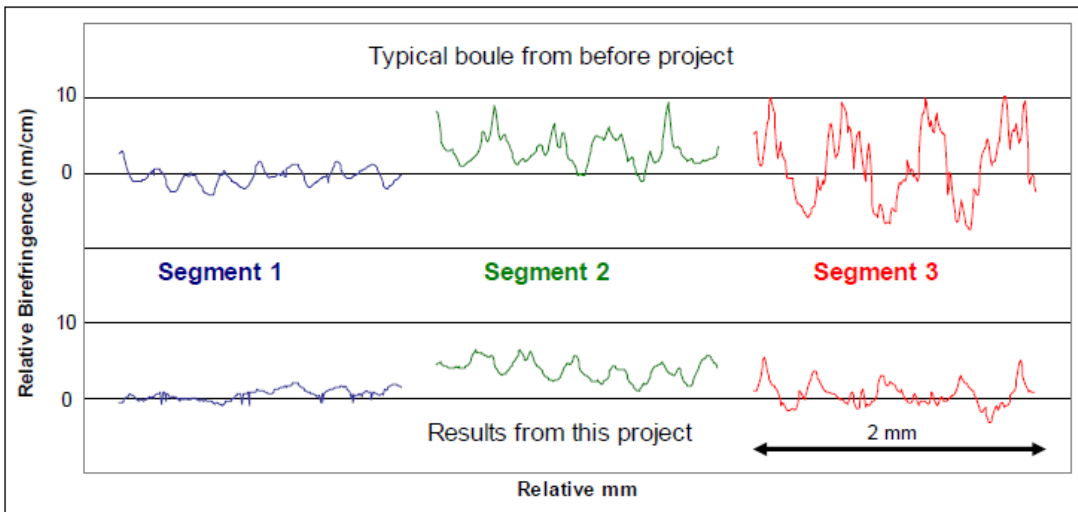
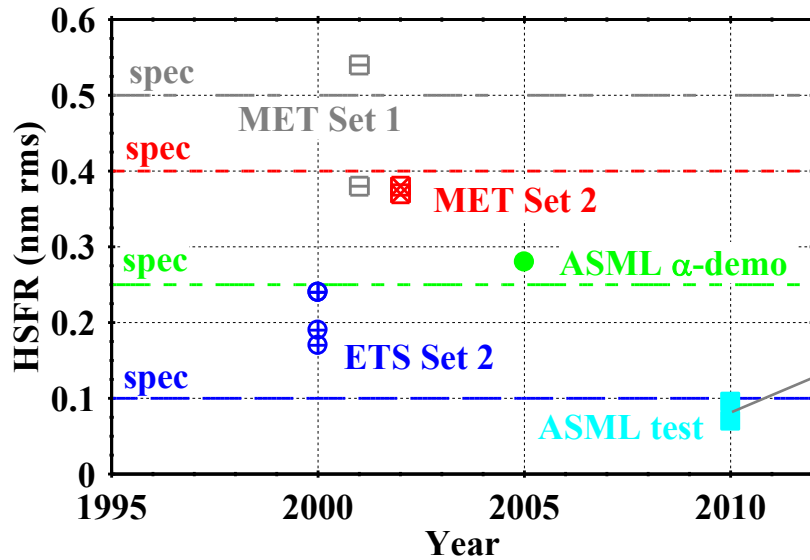
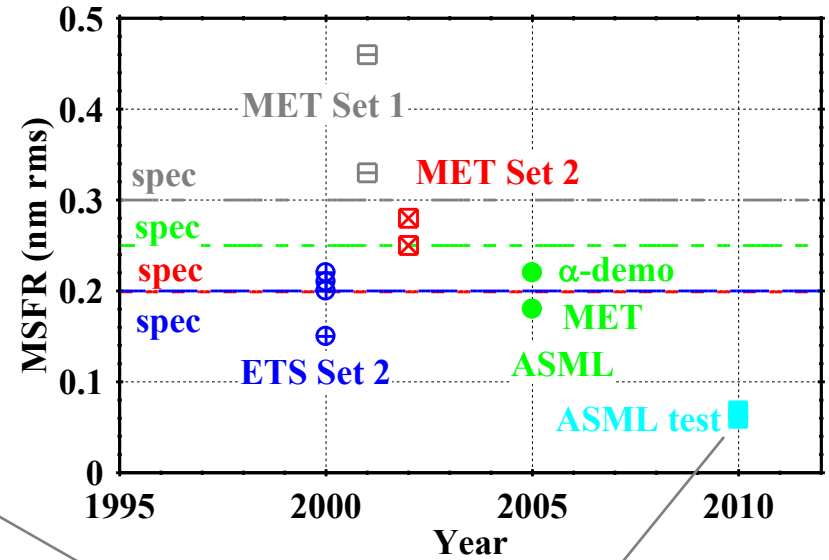
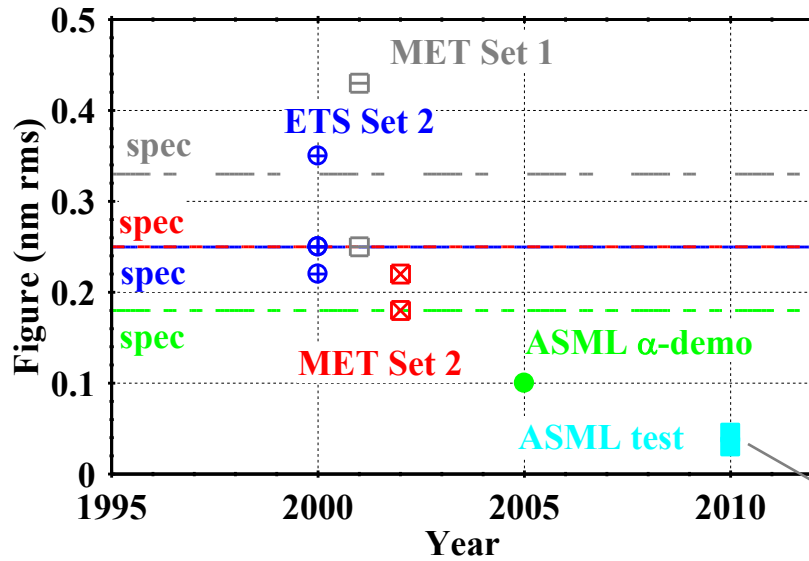


Figure 8: Striae differences showing a recently formed boule to one that was formed before this project was started.

Recent progress in diminishing striae is promising towards use of ULE for EUVL projection optics

W. Rosch, L. Beall, J. Maxon, R. Sabia, R. Sell, "Characterization of striae in ULE® for EUVL optics and masks" Proc. SPIE 6151, 615122 (2006).

# Historical evolution of figure, MSFR and HSFR of EUVL projection optics and comparison with specs



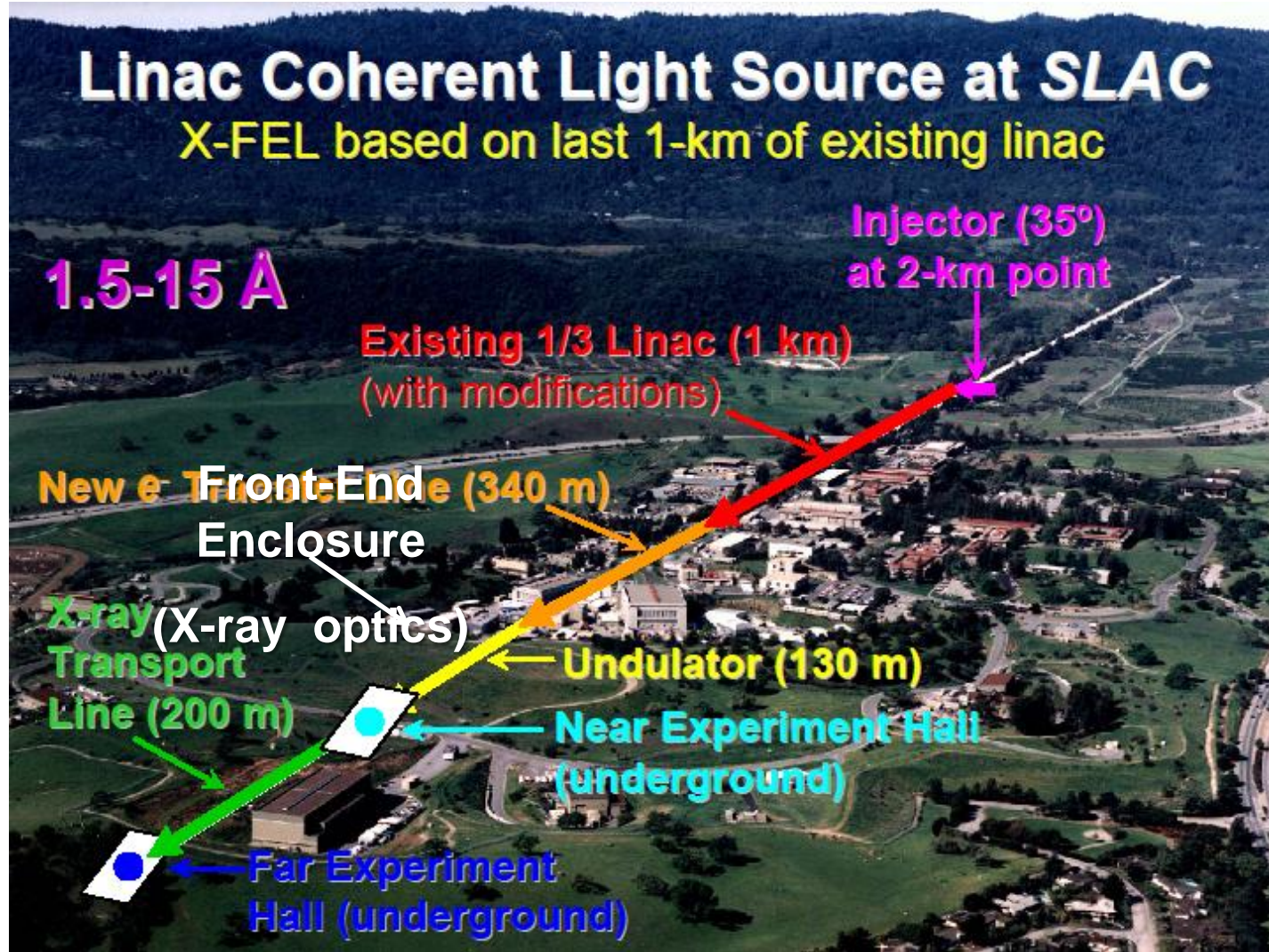
ULE??

R.Soufli, et al, Proc. SPIE 4343, 51-59 (2001).  
 U. Dinger, et al, Proc. SPIE 5193, 18-28 (2004).  
 H. Meiling, et al, Proc. SPIE 5751 90-101 (2005).  
 R. Soufli, et al, Appl. Opt. 46, 3736-3746(2007).  
 M. Lowisch, et al, Proc. SPIE 7636, 763603 (2010).





# The advance of x-ray Free Electron Laser (FEL) sources has pushed the limits of x-ray optics fabrication





# Si substrate specifications for the LCLS are driven by the need to preserve the coherence of the x-ray FEL beam

Error Category		Specification	Spatial Wavelength
Figure	Height Error	$\leq 2.0 \text{ nm rms}^\ddagger$	1 mm to Clear Aperture <sup>†</sup>
	Slope Error	$\leq 0.25 \text{ } \mu\text{rad rms}$	
Mid-Spatial Roughness		$\leq 0.25 \text{ nm rms}$	2 $\mu\text{m}$ to 1 mm
High-Spatial Roughness		$\leq 0.4 \text{ nm rms}$	20 nm to 2 $\mu\text{m}$

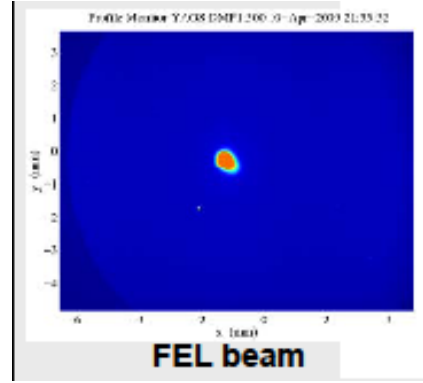
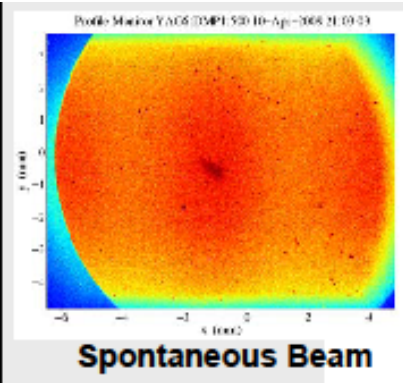
† **SOMS mirrors:** Flat, planar, 250×30×50 mm<sup>3</sup>, Clear Aperture = 175×10 mm<sup>2</sup>

† **HOMS mirrors:** Flat, planar, 450×30×50 mm<sup>3</sup>, Clear Aperture = 385×15 mm<sup>2</sup>

‡2 nm rms height error derived from Maréchal criterion: wavefront error <  $\lambda/14$  rms

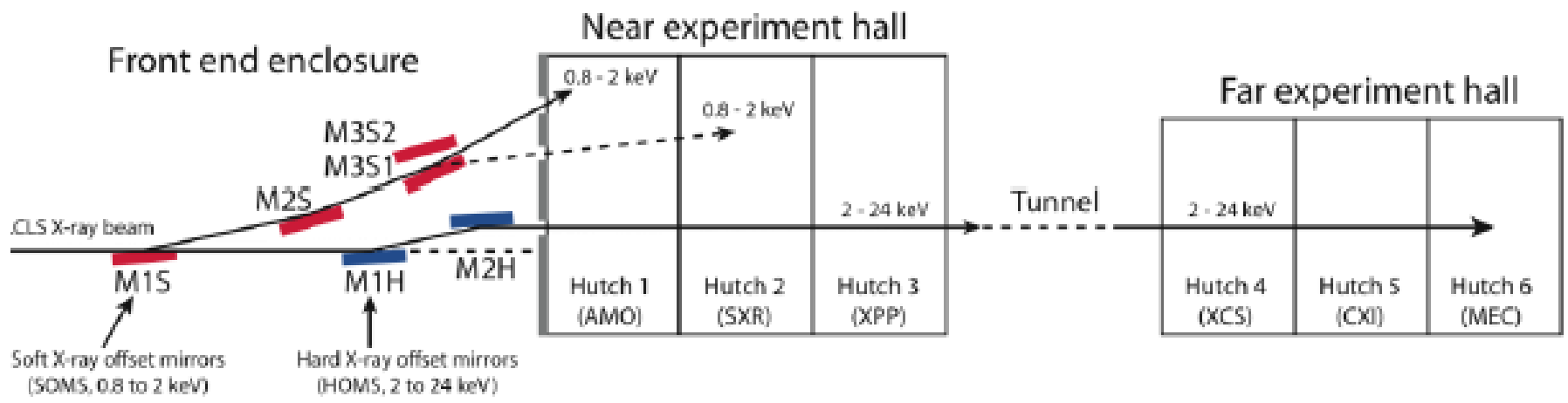
M. Pivovarov, R. M. Bionta, T. J. Mccarville, R. Soufli, P. M. Stefan, “Soft X-ray mirrors for the Linac Coherent Light Source”, Proc. SPIE 6705, 67050O (2007).

R. Soufli, M. J. Pivovarov, S. L. Baker, J. C. Robinson, E. M. Gullikson, T. J. McCarville, P. M. Stefan, A. L. Aquila, J. Ayers, M. A. McKernan, R. M. Bionta, “Development, characterization and experimental performance of x-ray optics for the LCLS free-electron laser” Proc. SPIE 7077, 707716 (2008).



➤ LLNL led the construction of the LCLS front-end enclosure x-ray optics and diagnostics, and developed coatings and metrologies for x-ray mirrors and gratings for the AMO, SXR, CXI and MEC beamlines

➤ About 20 diffraction-limited, grazing incidence x-ray mirrors (consisting of a Si substrate coated with B<sub>4</sub>C or SiC materials) will be ultimately installed at LCLS

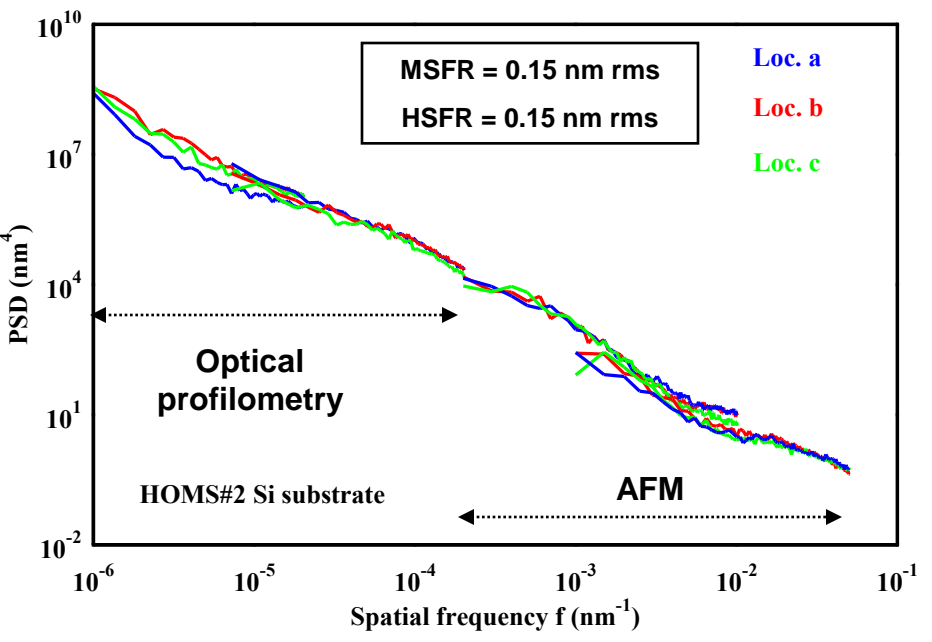
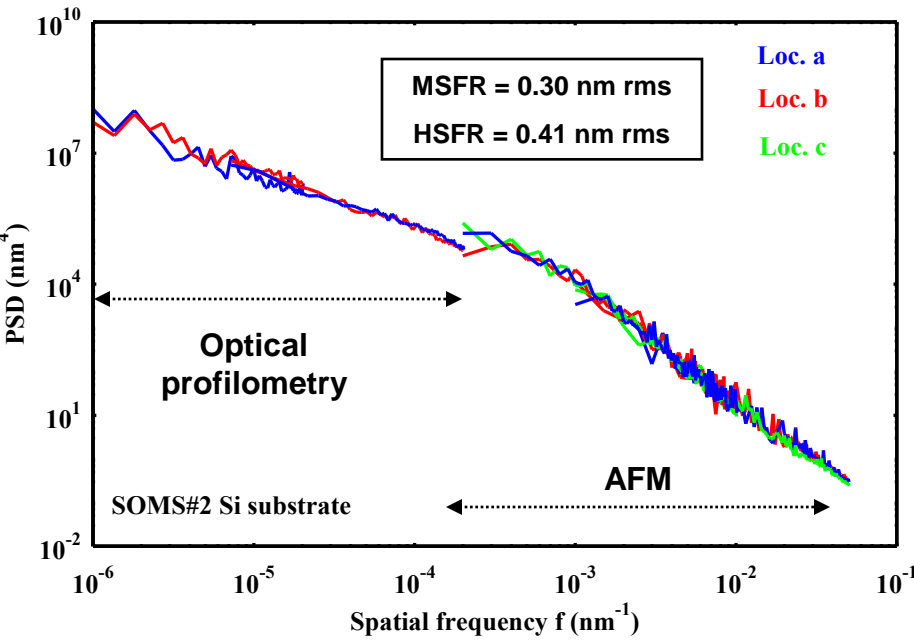


**Unique requirements for LCLS x-ray mirrors:**

- Withstand instantaneous peak power of LCLS FEL (B<sub>4</sub>C and SiC coating materials)
- Coherence/intensity preservation of LCLS wavefront (< 2 nm rms figure, 0.25 nm rms MSFR)
- Pointing stability and resolution (< 900 nrad for soft x-ray, < 90 nrad for hard x-ray mirrors)



# Diffraction-limited, grazing incidence Si substrates with EUVL-quality figure and finish have been manufactured for the LCLS x-ray FEL



Mirror #	Figure (nm RMS)	Slope error (μrad RMS)
SN1	1.8	0.19
SN2	1.3	0.2
SN3	1.2	0.37
SN4	0.64	0.14
SN5	1.4	0.37

Measured along central 200 mm

Mirror #	Figure (nm RMS)	Slope error (μrad RMS)
SN1	2.4	0.27
SN2	1.0	0.27
SN3	2.0	0.22
SN4	1.5	0.23

Measured along central 420 mm

*SOMS Si substrates manufactured by InSync (Albuquerque, New Mexico)*

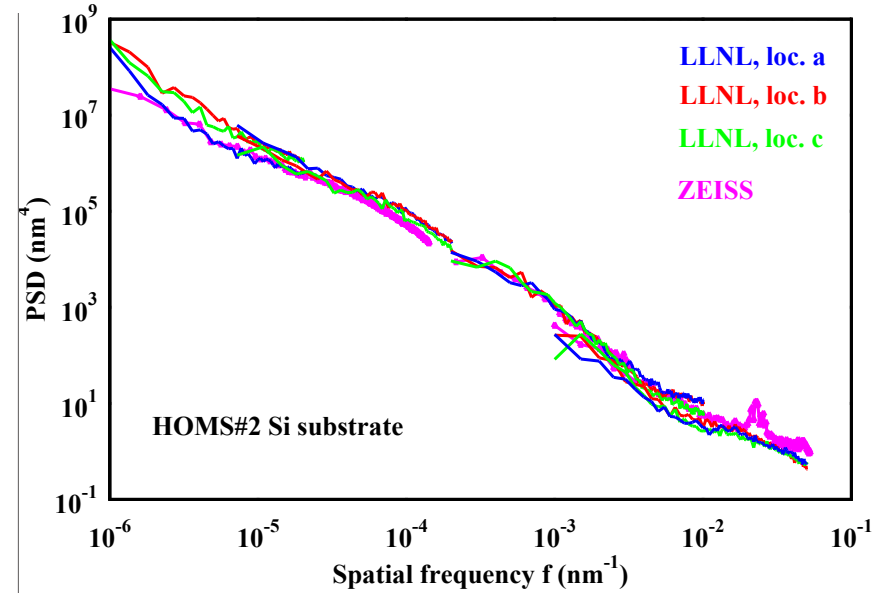
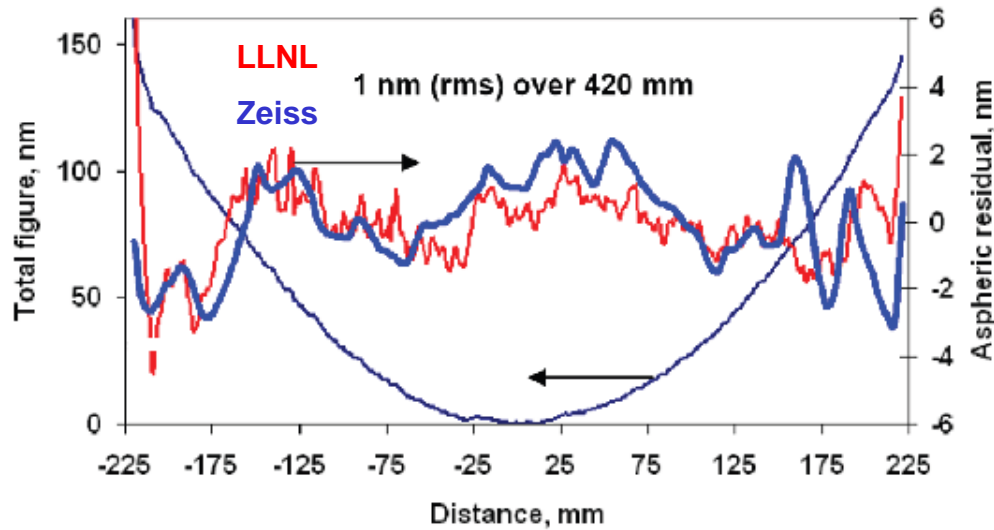
*HOMS Si substrates manufactured by Carl Zeiss Laser Optics (Oberkochen, Germany)*

A. Barty, R. Soufli, T. McCarville, S. L. Baker, M. J. Pivovarov, P. Stefan and R. Bionta, "Predicting the coherent X-ray wavefront focal properties at the Linac Coherence Light Source (LCLS) X-ray free electron laser", Optics Express 17, 15508-15519 (2009)





# Recent cross-validation of LLNL and Zeiss metrology in the figure, MSFR and HSFR



*Zeiss measurements courtesy of Helge Thiess, Carl Zeiss Laser Optics*

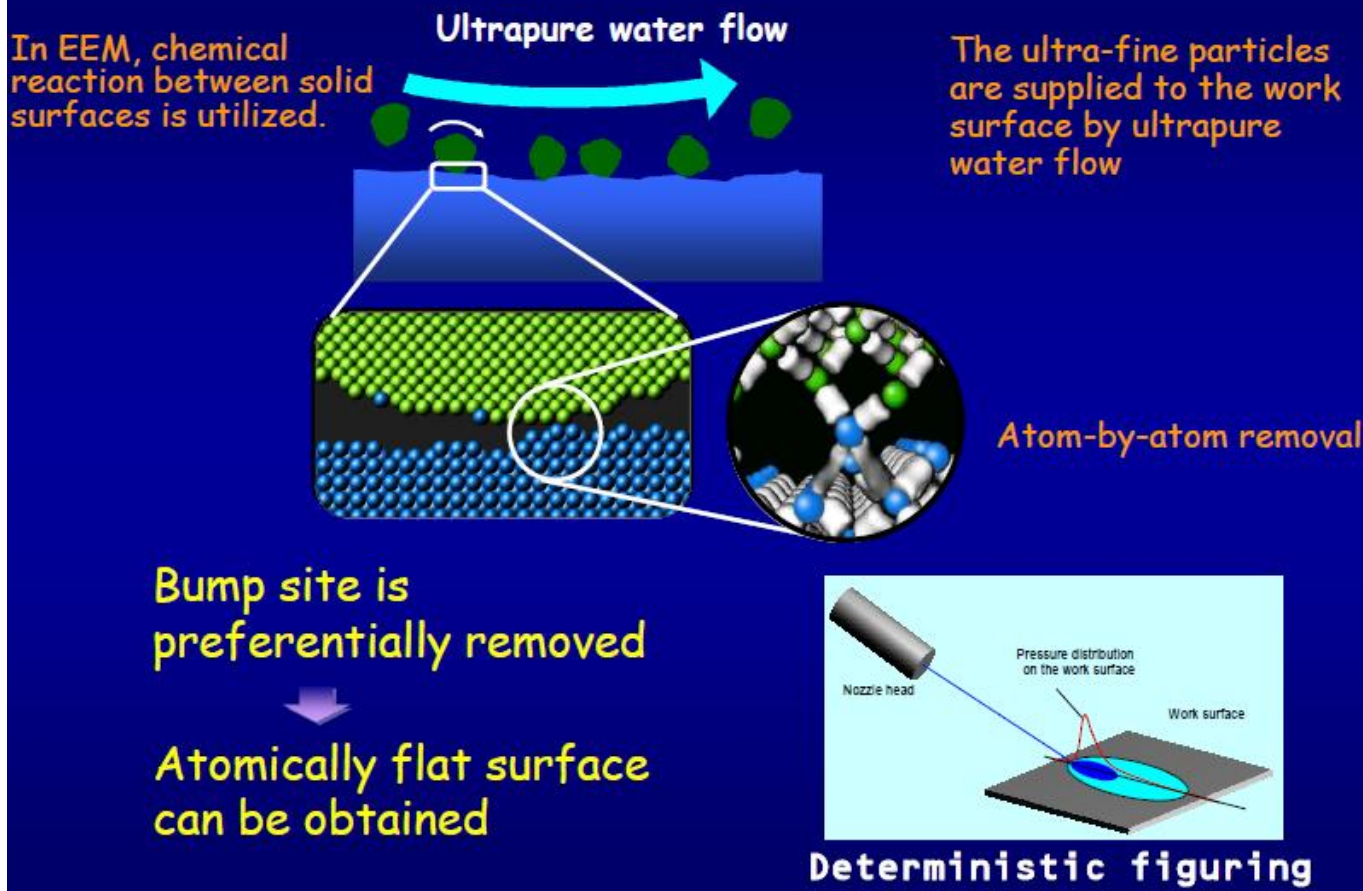
# EUVL could also benefit from novel, advanced polishing techniques developed for synchrotron and FEL optics



Courtesy: Prof. Kazuto Yamauchi (Osaka University)

## Removal mechanism of EEM (Elastic Emission Machining)

6



K.Yamauchi et al, Rev. Sci. Instrum. 73 2028 (2002).

# Si substrate for the LCLS FEL, polished by EEM



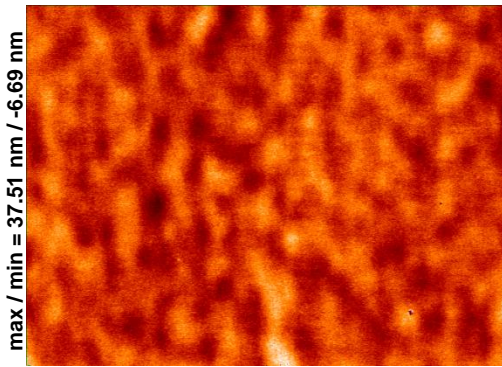
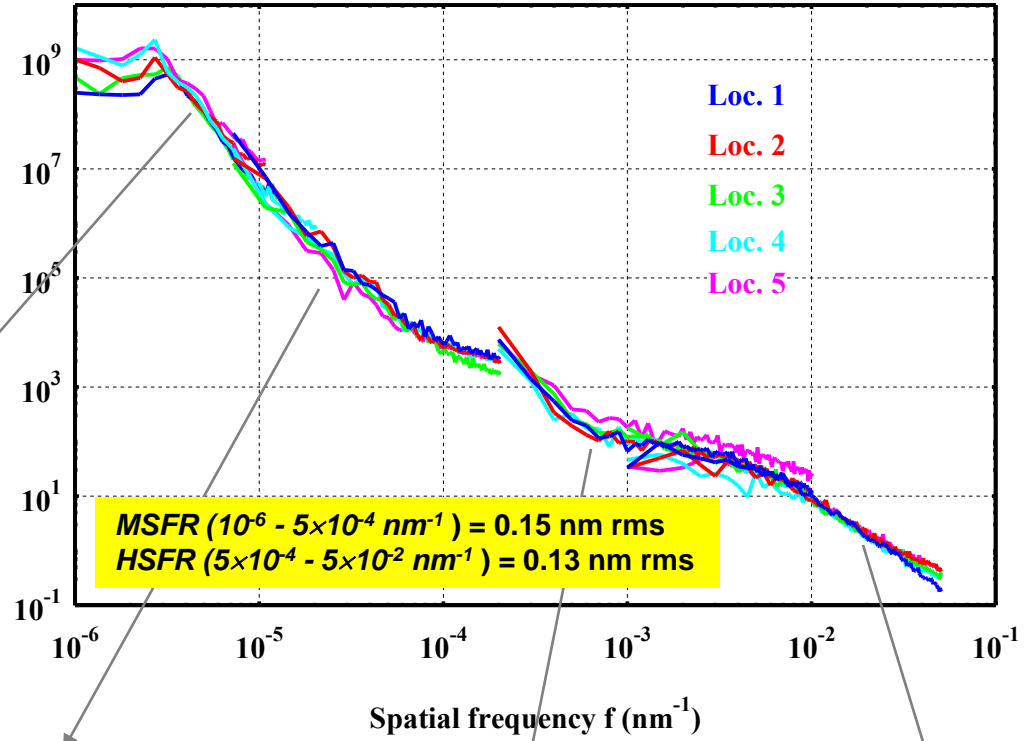
CXI KB1 Si substrate



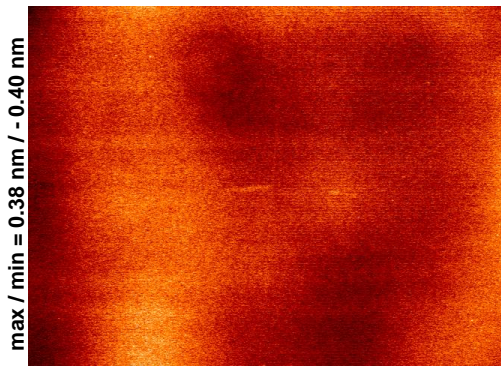
Figure of ~ 1 nm rms along 350 mm was measured at BESSY (Frank Seiwert)

370 mm

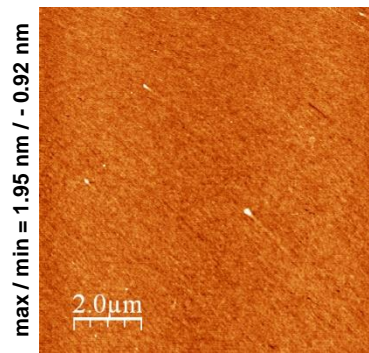
PSD ( $\text{nm}^4$ )



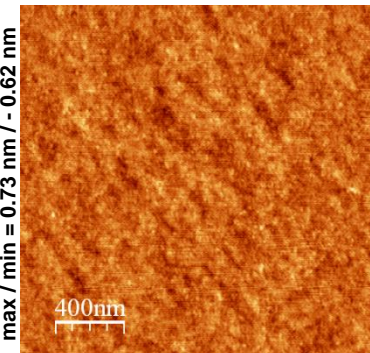
2.95 mm  
Zygo 2x



0.37 mm  
Zygo 20x



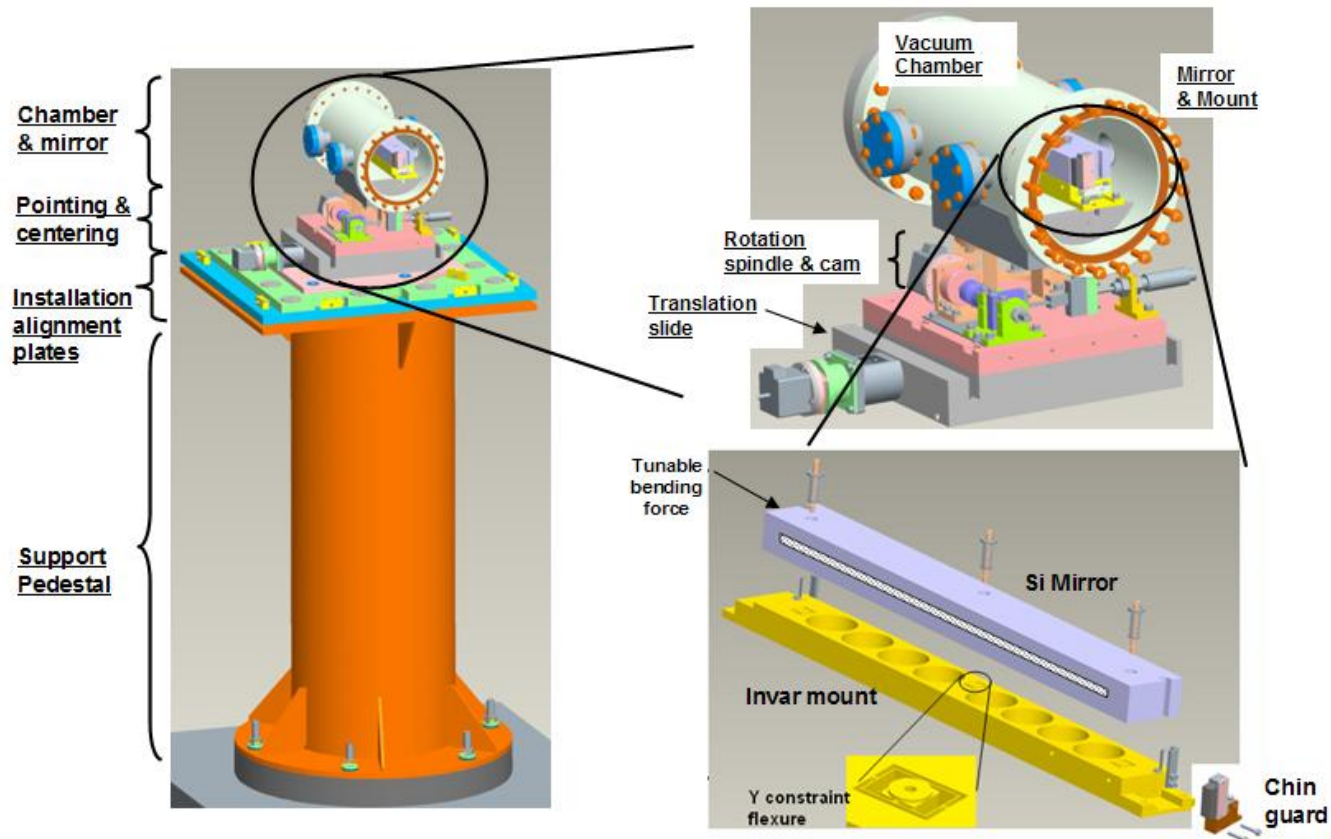
10 μm  
AFM



2 μm  
AFM



# Novel concepts in x-ray mirror mounting, installation and alignment at LCLS



- T-controlled enclosure demonstrates  $\pm 0.01$  °C temperature and  $\pm 30$  nrad HOMS pointing stability
- Hard x-ray mirror figure can be remotely controlled

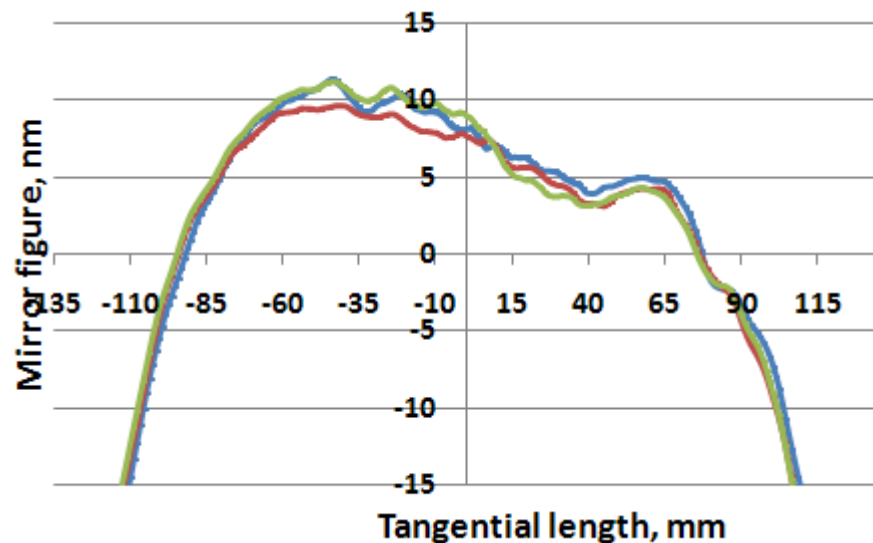
T. J. McCarville, P. M. Stefan, B. Woods, R. M. Bionta, R. Soufli, M. J. Pivovarov, "Opto-mechanical design considerations for the Linac Coherent Light Source X-ray mirror system", Proc. SPIE 7077, 70770E (2008).



# LCLS soft x-ray mirror figure is maintained after coating and mounting



### Total Figure

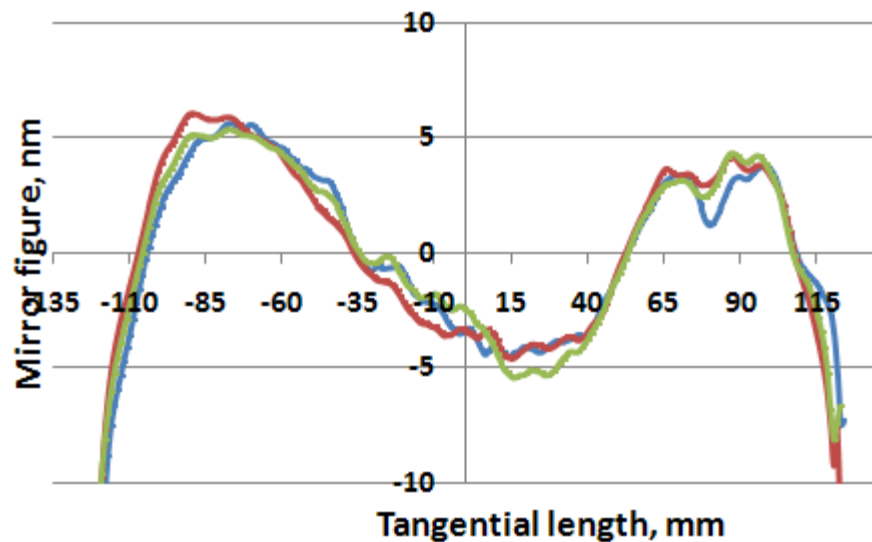


Before coating

Coated, un-mounted

Coated & mounted

### Aspheric residual (sphere subtracted)

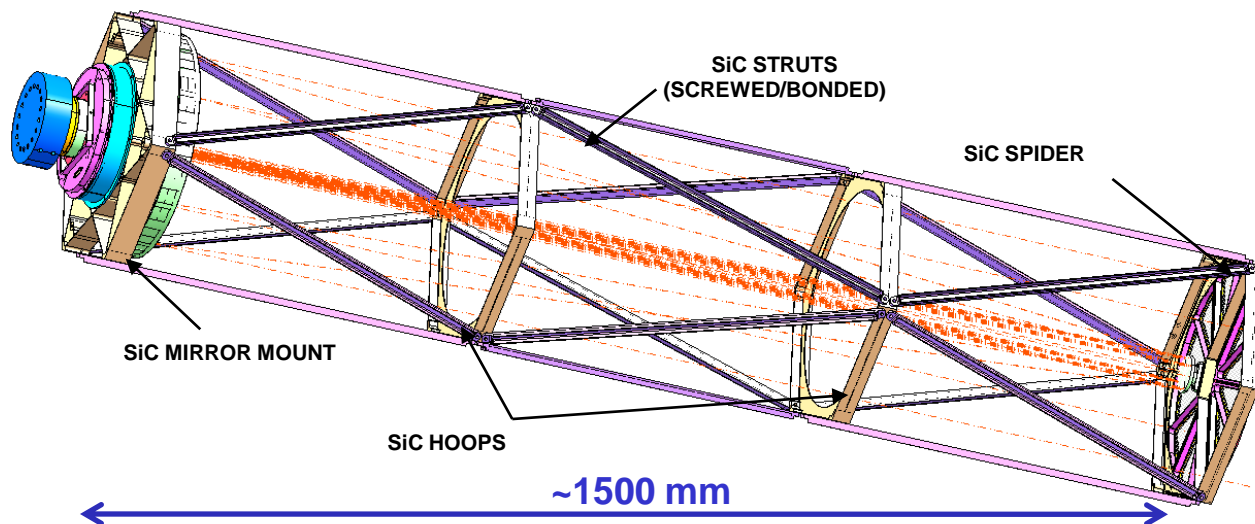


Before coating: 1.81 nm & 0.19  $\mu$ rad rms  
over central 200 mm

Coated, un-mounted: 1.62 nm & 0.173  $\mu$ rad rms

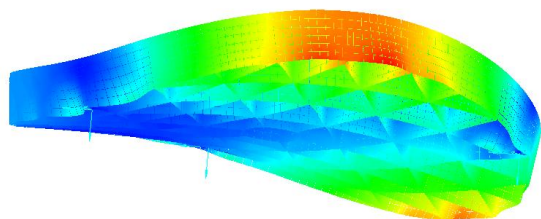
Coated & mounted: 1.88 nm & 0.18  $\mu$ rad rms

# Silicon Carbide (SiC) has emerged as a viable material for EUV/x-ray space telescope and synchrotron optics



**HiLiTE:** a 300-mm aperture Cassegrain telescope design made entirely of SiC, including optical substrates and metering structure. Overall mass is **4X lighter** than the mass of an equivalent conventional telescope

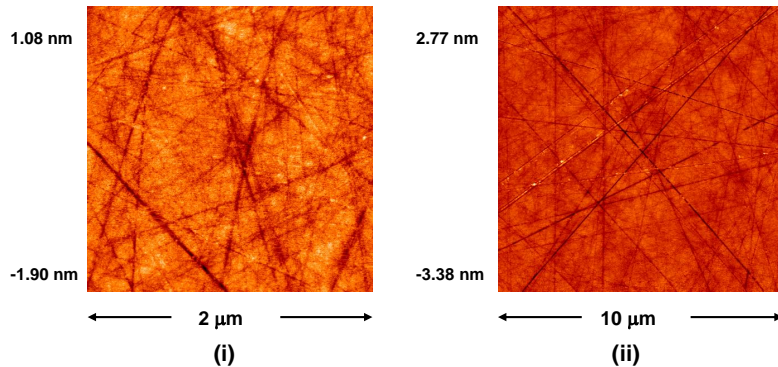
MODE: 1      FREQ: 1487.052  
 DISPLACEMENT - MAG MIN: 0.00E+00 MAX: VAL: 0.00E+00 POSITION: ACTUAL  
 FRAME OF REF: PART



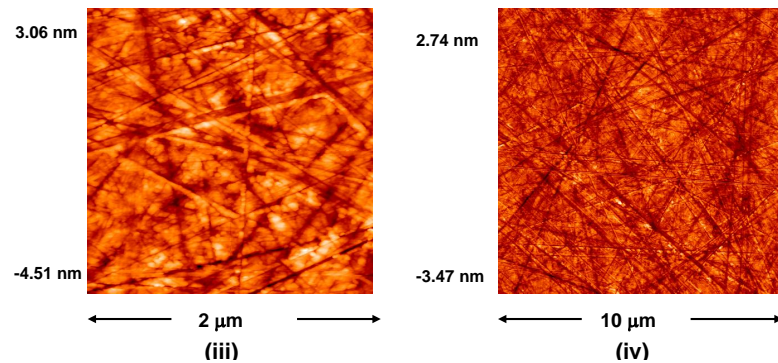
	System
Effective Focal Length	10.313 m
Focal Ratio	f/34
Plate Scale	20 arcsec/mm
Field of View	> 4x4 arcmin*
	<b>Primary Mirror</b>
Clear Aperture	300 mm
Radius of Curvature	- 3564.2564 mm
Conic	- 1
	<b>Secondary Mirror</b>
Clear Aperture	40 mm
Radius of Curvature	- 680.89795 mm
Conic	- 2.0116

D. S. Martínez-Galarce, P. Boerner, R. Soufli, B. De Pontieu, N. Katz, A. Title, E. M. Gullikson, J. C. Robinson, S. L. Baker, "The high-resolution lightweight telescope for the EUV (HiLiTE)", Proc. SPIE 7011 , 70113K (2008).

# Fabrication and polishing techniques for SiC optical substrates



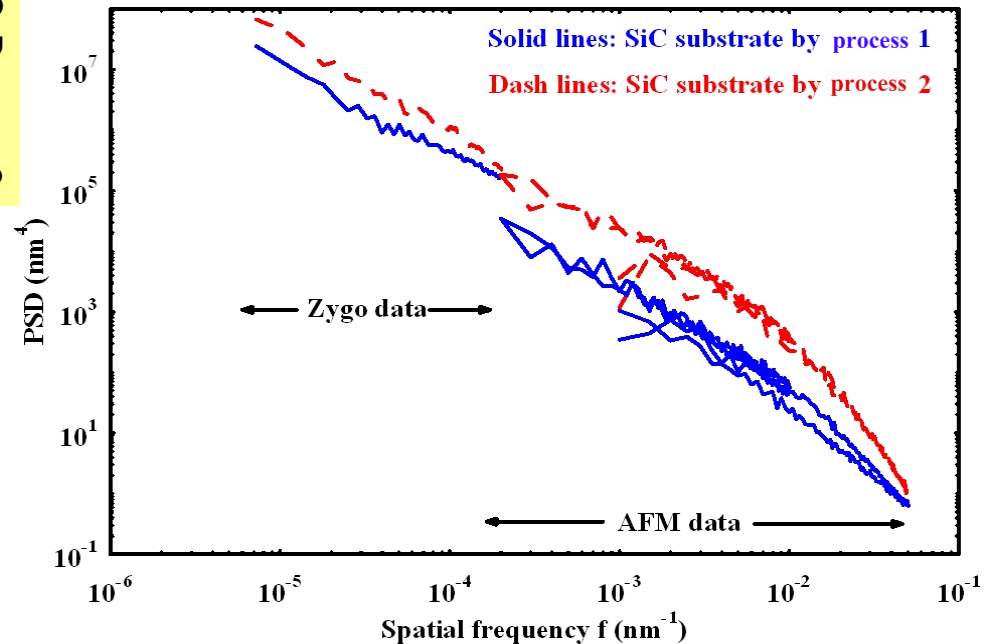
SiC, Process 1



SiC, Process 2

	<b>HSFR</b> $0.05 \mu\text{m} < \Lambda < 2 \mu\text{m}$
<b>Process 1</b>	<b>0.30 nm rms</b>
<b>Process 2</b>	<b>0.84 nm rms</b>

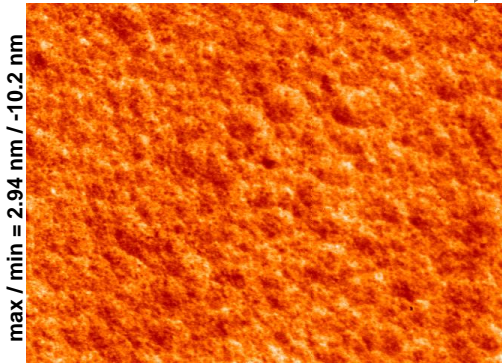
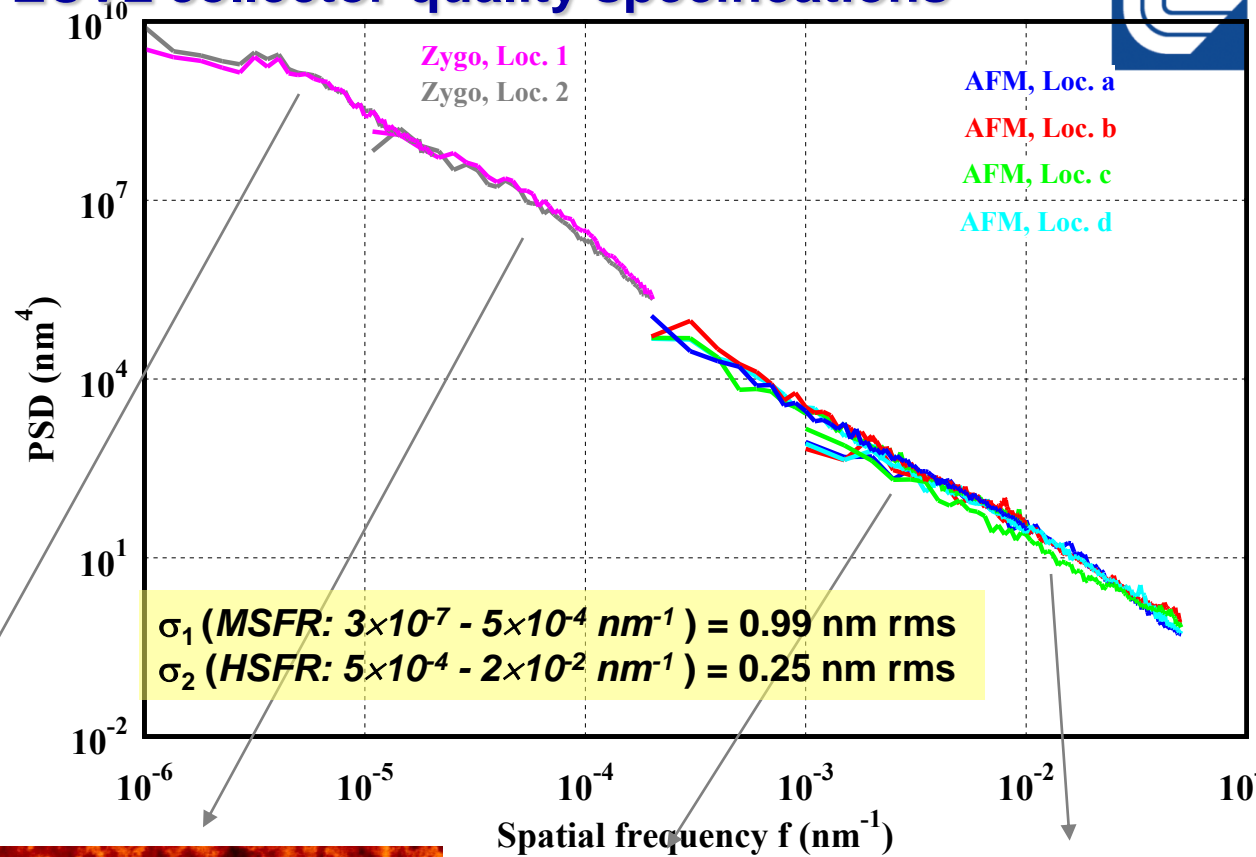
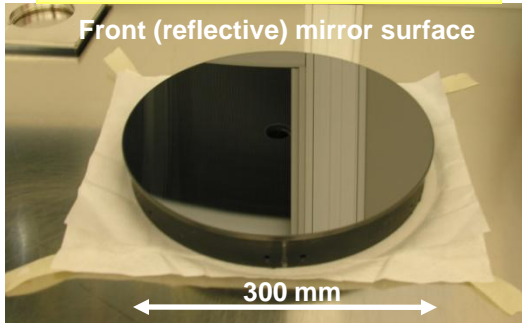
- Start with bulk SiC, deposit SiC “cladding” using using a CVD-type process
- Or: deposit SiC entirely using a CVD-type process
- Polish using mechanical grind/polish, reactive atom plasma etching, or other technique



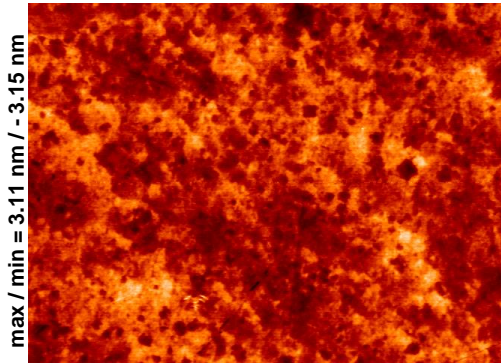
# SiC could be polished to EUVL collector-quality specifications



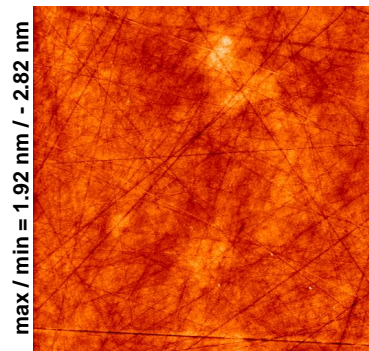
Test mirror for space telescope



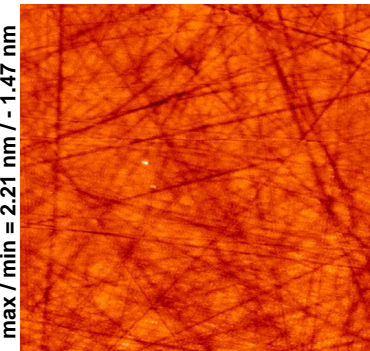
2.95 mm  
Zygo 2x



0.37 mm  
Zygo 20x



10  $\mu\text{m}$   
AFM



2  $\mu\text{m}$   
AFM



# Other SiC-based ceramic composite materials could be considered for EUVL collector substrates

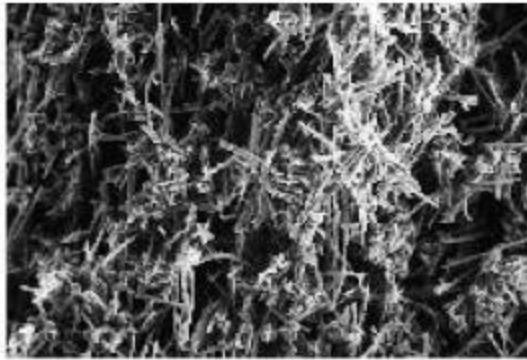
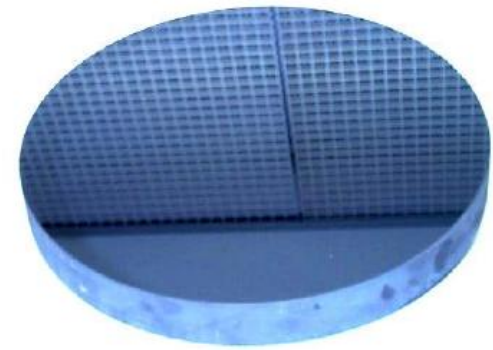
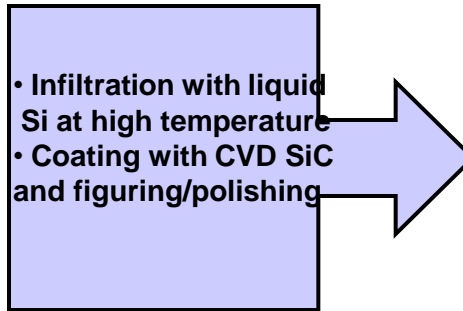


Fig. 2 REM microphotograph of the greenbody chopped C/C fiber material



300 mm

- Novel SiC-based ceramic composite materials have been developed for space optical substrates and structures
- Materials are lightweight, with high stiffness, high conductivity and low CTE
- Feasibility of achieving figure/finish quality to EUVL collector specifications would have to be verified



M. R. Kroedel, "Cesic®-Engineering material for optics and structures" Proc. SPIE 5868, 58680A (2005).  
M. R. Kroedel and T. Ozaki, "HB-Cesic Composite for Space Optics and Structures", Proc. SPIE 6666, 66660E (2007).  
M. Strahan *et al*, "Novel technologies for large deformable mirrors", Proc. SPIE 7736, 773664 (2010).

# **EUVL collector optics have more relaxed figure and MSFR specs compared to projection optics and can be fabricated using low-cost techniques**



- **Aspherical mirrors made by conventional figuring / finishing are very expensive**
- **Diamond-turned (metal) or ground (ceramic) mirrors are much cheaper and meet EUVL collector figure specs but have insufficient high-spatial frequency roughness (HSFR)**

## **Proposed solution:**

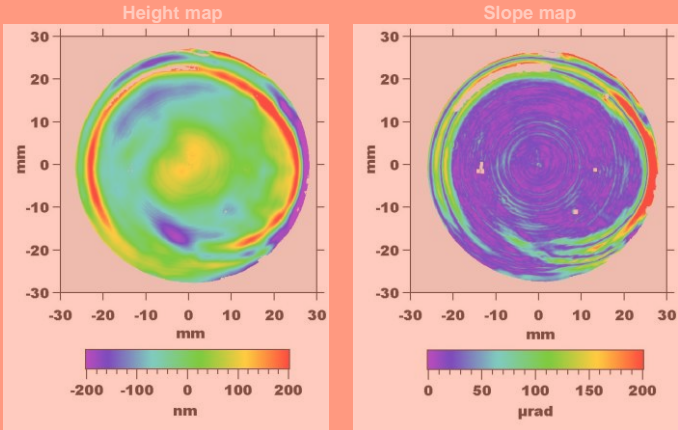
- **Fabricate diamond-turned metal (e.g. Al, Cu) or ground ceramic (e.g. SiC) mirrors**
- **Reduce HSFR with smoothing film**
- **Follow with appropriate coating (single-layer or multilayer) for EUV reflectance**

**J. A. Folta, C. Montcalm, J. S. Taylor, E. A. Spiller, “Low-cost method for producing extreme ultraviolet lithography optics”, U.S. Patent No. 6,634,760.**

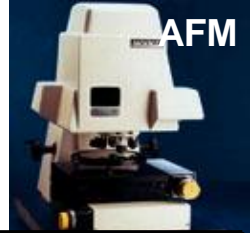
# Polyimide-smoothing of diamond-turned Al EUVL collector substrates dramatically improves HSFR while maintaining figure within specs



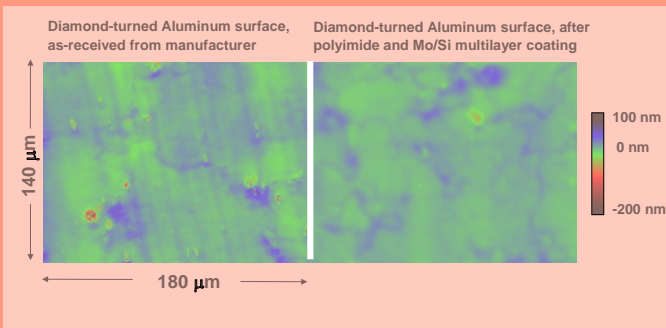
Visible light interferometry results from multilayer-coated, diamond-turned condenser mirror



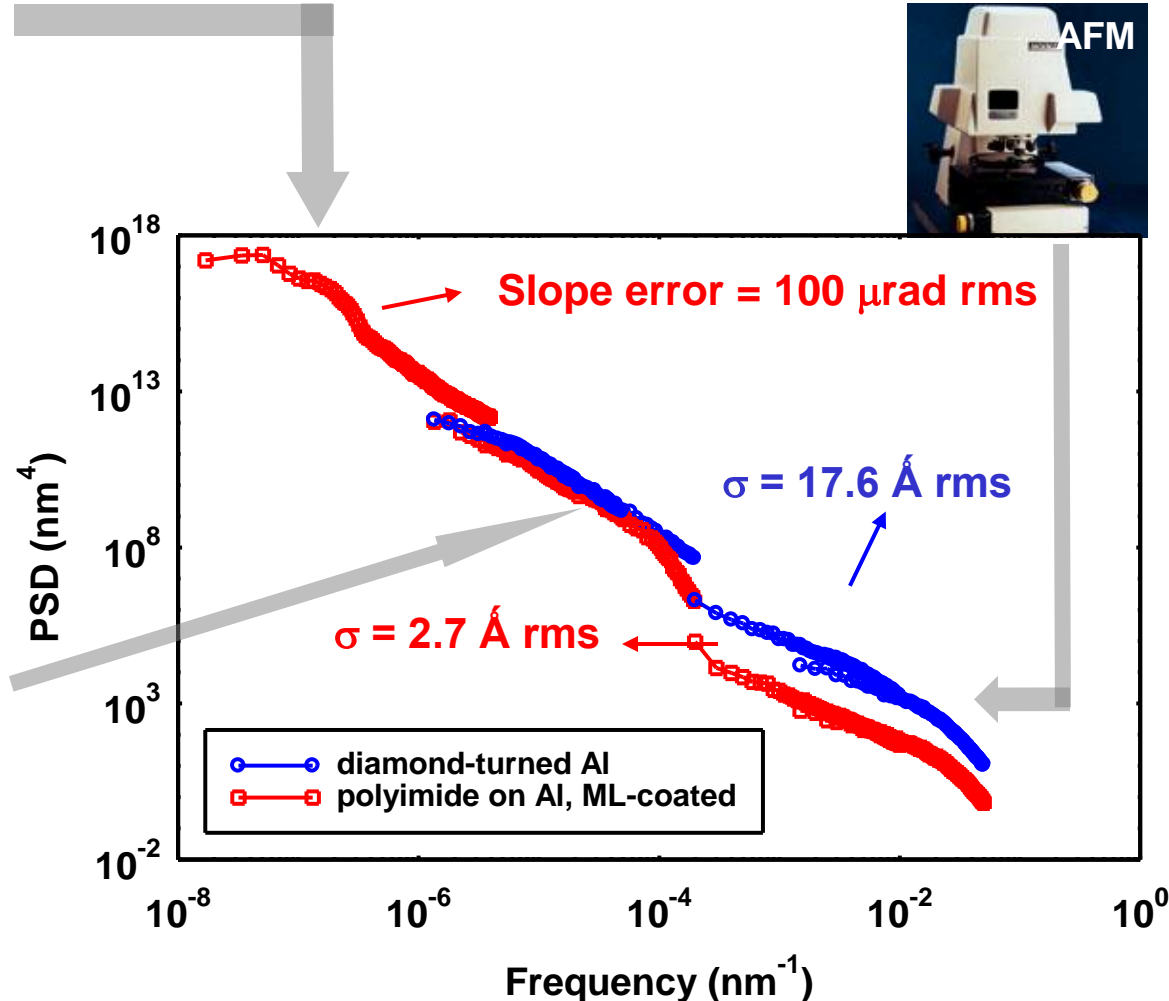
R. Soufli, E. Spiller, M. A. Schmidt, J. C. Robinson, S. L. Baker, S. Ratti, M. A. Johnson, E. M. Gullikson, *Opt. Eng.* 43(12), 3089-3095 (2004).



Polyimide smoothes high spatial frequency roughness, including 10 μm-range diamond turning marks



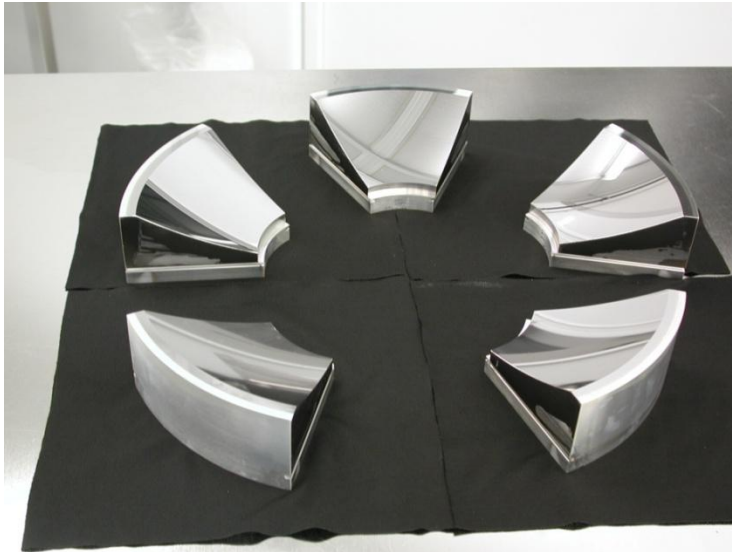
Measurements obtained with a Zygo New View™ optical profiling microscope operated at 40x objective lens magnification



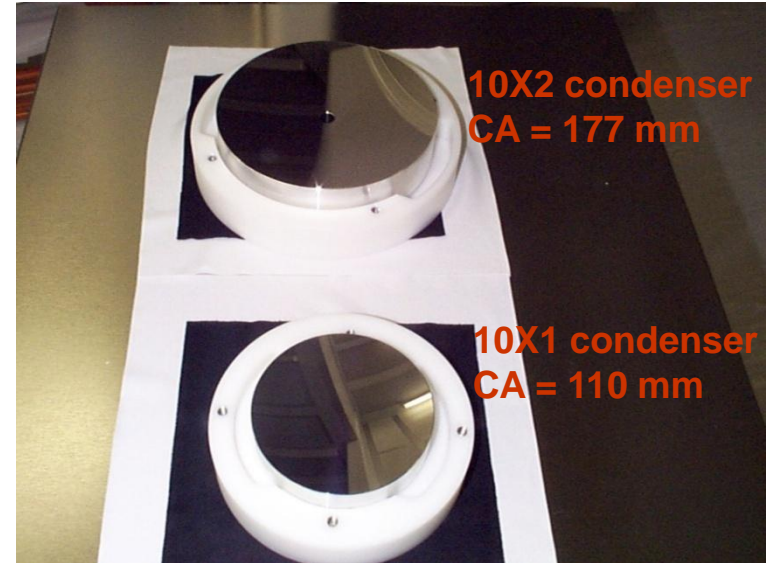
# Diamond-turned, polyimide-smoothed EUVL condenser optics developed at LLNL



## C1 collector optic for the ETS

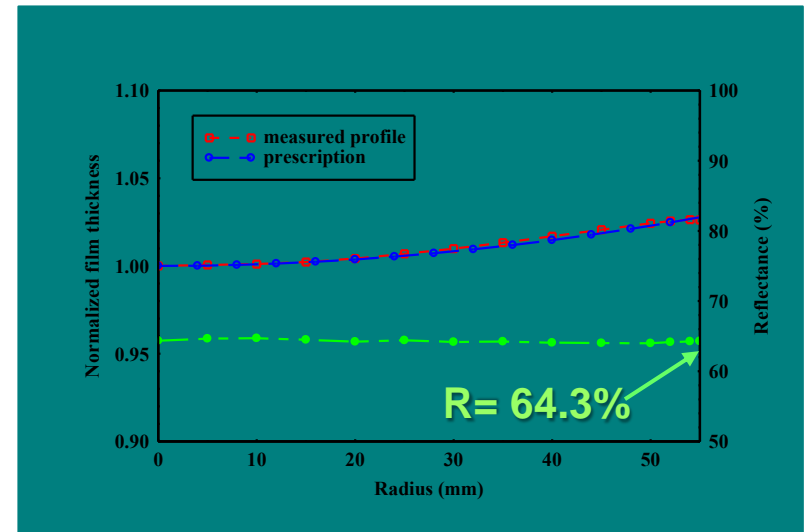


## Illuminator optics for SNL microstepper



➤ HSFR is reduced from ~3 nm to ~0.3 nm, and 64.3 % reflectance is achieved at 13.35 nm and 8 deg off-normal, after Mo/Si multilayer coating

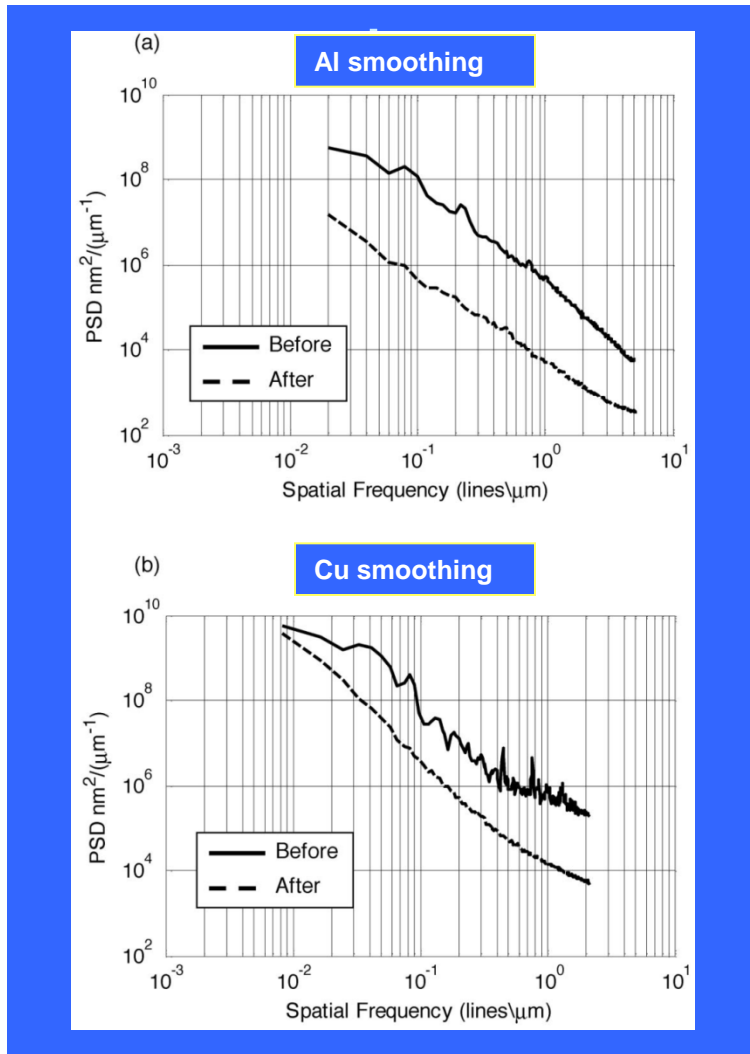
➤ No accelerated degradation or outgassing were observed, when exposed to 11.5M shots of EUVL laser-plasma source environment (Xe liquid jet source at SNL)







# Smoothing of diamond-turned Cu and Al condenser optics with spin-on-glass resist was also demonstrated at CXRO/LBNL



➤ HSFR is reduced from  $\sim 3.3 - 3.7$  nm to  $\sim 0.4 - 0.6$  nm, and 64-65 % reflectance is achieved at 13.50 nm and 28 deg off-normal, after Mo/Si multilayer coating

➤ Mo/Si-coated, smoothed optics are used as illuminator mirrors for MET beamline at LBNL



F. Salmassi, P. P. Naulleau, and E. M. Gullikson, "Spin-on-glass coatings for the generation of superpolished substrates for use in the extreme-ultraviolet region", Appl.Opt. 45, 2404-2408 (2006).



# Perspectives on 6.x nm lithography

- A PO system with near-zero as-designed wavefront error will be required
- Phase change through multilayer stack vs. angle of incidence is expected to be more severe at 6.x nm than 13 nm, therefore:
  - ❖ Differences between actinic and non-actinic inspection will be larger
  - ❖ Actinic qualification of PO boxes may be required
- Flare requirements lead to MSFR specifications beyond the state-of-the-art in polishing technologies
- Reflectance and bandwidth of 6.x nm multilayers will need to be greatly improved. Recently determined, experimental optical constants for B and B<sub>4</sub>C are available to model the performance of B- and B<sub>4</sub>C-based multilayers. See next 2 slides and also presentations by V. Banine, E. Louis and Y. Platonov
- Source, resist - see also presentation by V. Banine
- Extensive and coordinated synergy between industry, universities and research institutes would be required to successfully address the above issues

# Photoabsorption measurements yield updated values for the EUV/x-ray refractive index of B<sub>4</sub>C films, including NEXAFS

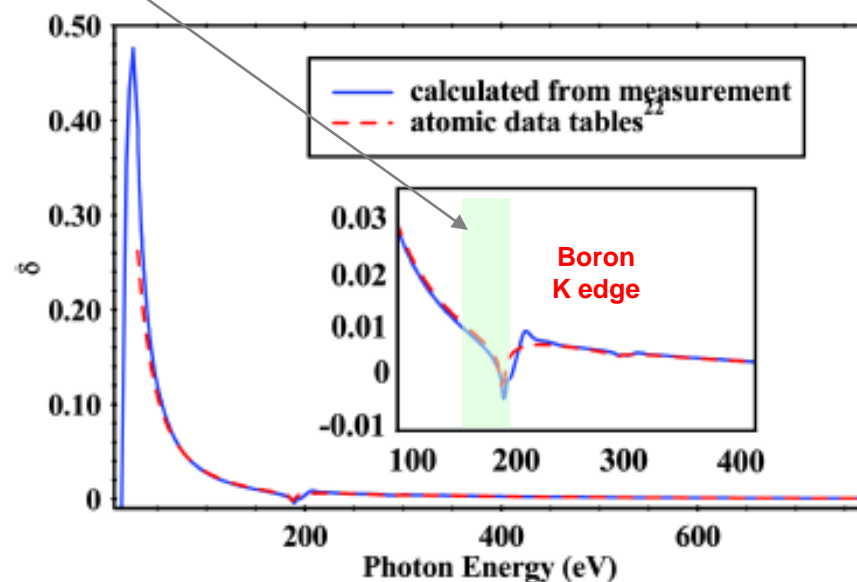
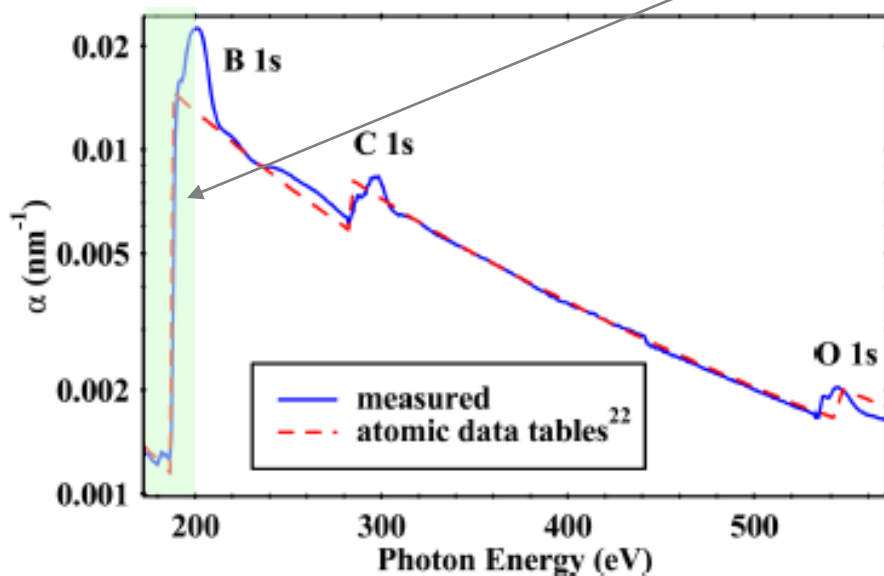


Accurate values of the refractive index (optical constants) enable accurate modeling of multilayer performance

$$n(\lambda) = 1 - \delta(\lambda) + ik(\lambda)$$

$$k(\lambda) = \lambda\alpha / 4\pi$$

Energy region of interest for 6.x nm, B<sub>4</sub>C-based multilayers



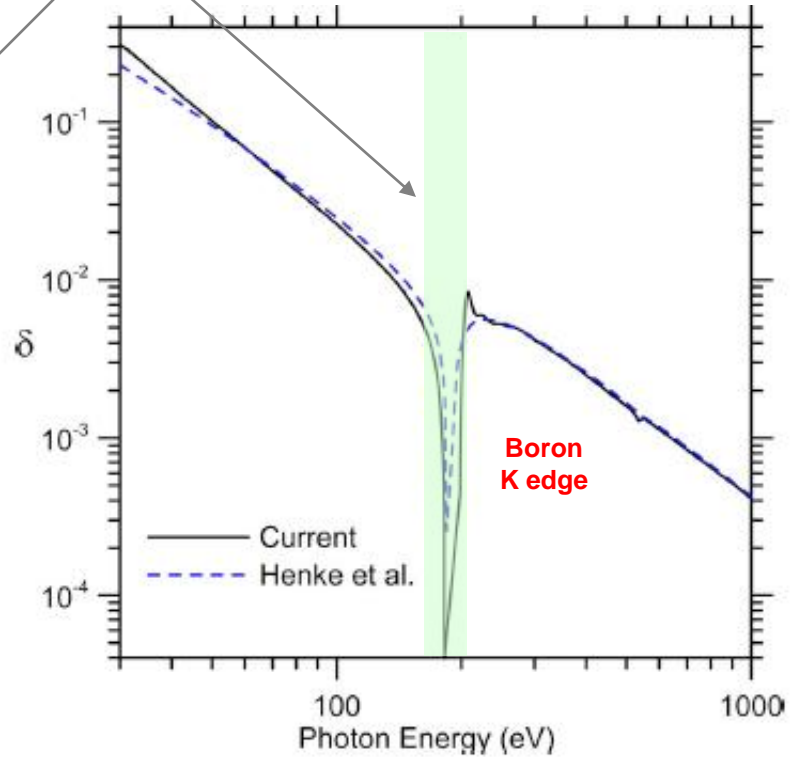
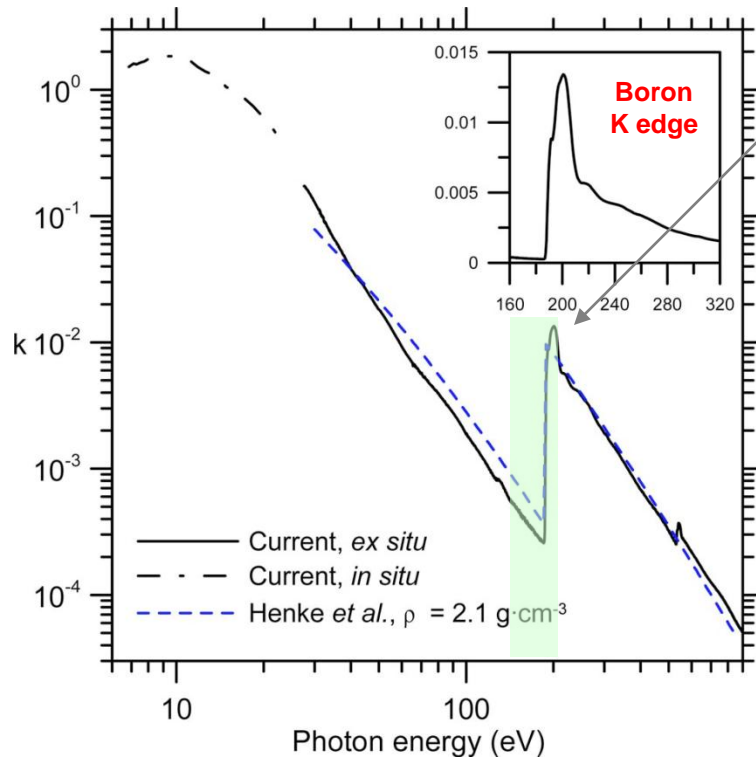
R. Soufli, A. L. Aquila, F. Salmassi, M. Fernández-Perea, E. M. Gullikson, "Optical constants of magnetron sputtered boron carbide thin films from photoabsorption data in the range 30 to 770 eV", Appl. Opt. 47, 4633-4639 (2008).

# We have also determined experimentally the Boron optical constants



$$n(\lambda) = 1 - \delta(\lambda) + ik(\lambda)$$

Energy region of interest for 6.x nm, B-based multilayers



M. Fernandez-Perea, J. I. Larruquert, J. A. Aznarez, J. A. Mendez, M. Vida-Dasilva, E. Gullikson, A. Aquila, R. Soufli, and J. L. G. Fierro, "Optical constants of electron-beam evaporated boron films in the 6.8-900 eV photon energy range", *J. Opt. Soc. Am. A*, 24(12), 3800-3807 (2007).





# Summary and conclusions

- One of EUVL's most significant technology accomplishments has been the fabrication and metrology of the world's most accurate normal-incidence optics
- Needs for higher throughput, lower flare and the ever increasing size and complexity of projection optical surfaces in advanced EUVL systems continues to push the limits of fabrication and metrology to picometer (pm) levels
- Overcoming manufacturing challenges may enable ULE to be used for EUVL projection optics substrates and achieve pm-level figure and roughness
- EUVL collector substrate technologies could benefit from recent advances in polishing/metrology/mounting of Si, SiC and other ceramic materials for FEL and space optics



# Funding acknowledgements

- The EUVL results in this presentation have been obtained through collaboration between researchers at Lawrence Livermore, Lawrence Berkeley and Sandia National Laboratories. Funding was provided by the EUV LLC (through a Cooperative Research and Development Agreement) and by Sematech
- Funding for the AIA/SDO EUV multilayer optics was provided by the Smithsonian Astrophysical Observatory
- Funding for the SUVI/GOES-R space weather satellite optics was provided by Lockheed Martin Corporation
- Other funding was provided by Lockheed Martin Corporation Internal Research and Development
- Funding for the LCLS optics was provided by SLAC National Accelerator Laboratory – US Department of Energy