

In-situ Cryogenic Cleaning Techniques for Tin-Contaminated EUV Mirrors

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Goal: Develop new tin-cleaning schemes for the EUV collector

Tests: Examine removal of tin droplet splats from EUV mirrors

Motivation: Tin- Cleaning of EUV Collector

- Considerable contamination of the collector mirror occurs by tin debris
- Chip manufacturing needs increased source availability and productivity
- Increase of collector lifetime needed: more than several months, > 400 Gp
- Internal tin-cleaning by plasma etching is too slow for thick deposits
- Improved tin-cleaning efficiency can increase uptime and reduce costs



Dripping Molten Tin Drops onto EUV Mirrors

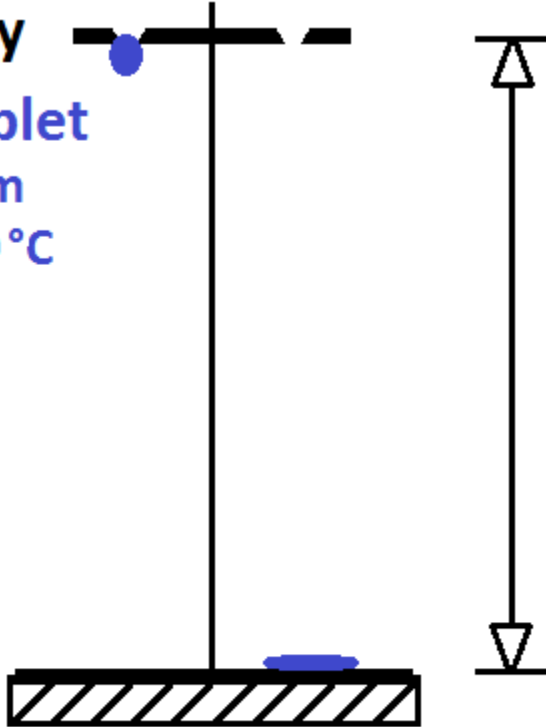
Tin dripping scheme:

Drip Tray

Tin Droplet

$D \sim 3\text{mm}$

$T_d \sim 250^\circ\text{C}$



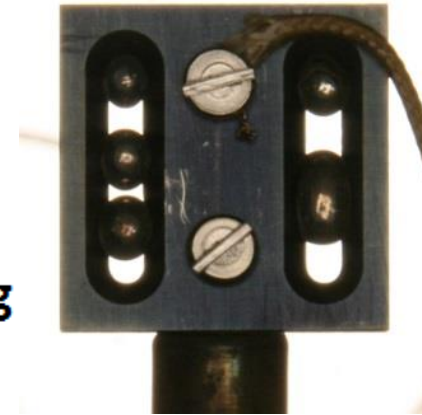
Mass of Tin Drop $m \sim 0.1\text{g}$

Drip Distance $d \sim 45\text{ cm}$

Dripping Time $t \sim 0.3\text{ s}$

Impact Velocity $v \sim 3\text{ m/s}$

Weber Number ~ 300



Sample,
heated or
cooled

Tin Splat
 $D \sim 10\text{ mm}$

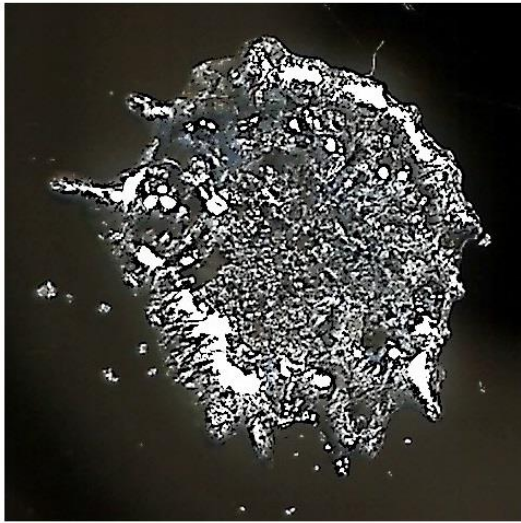
$T_s \sim 90^\circ\text{C}, 23^\circ\text{C}, -50^\circ\text{C}$

Regime: tin dripping below droplet splashing threshold, radial „finger“ pattern developing at edge of splat



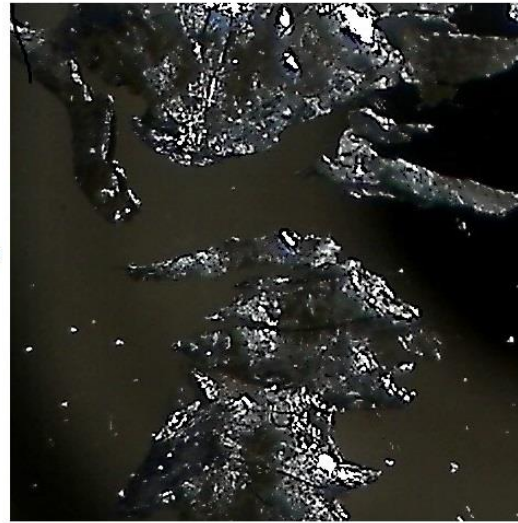
Phase Transformation of Tin Drop by Cooling

Induction of tin pest leads to embrittlement of tin-drop contamination



Contamination

=>



Phase Transition

=>



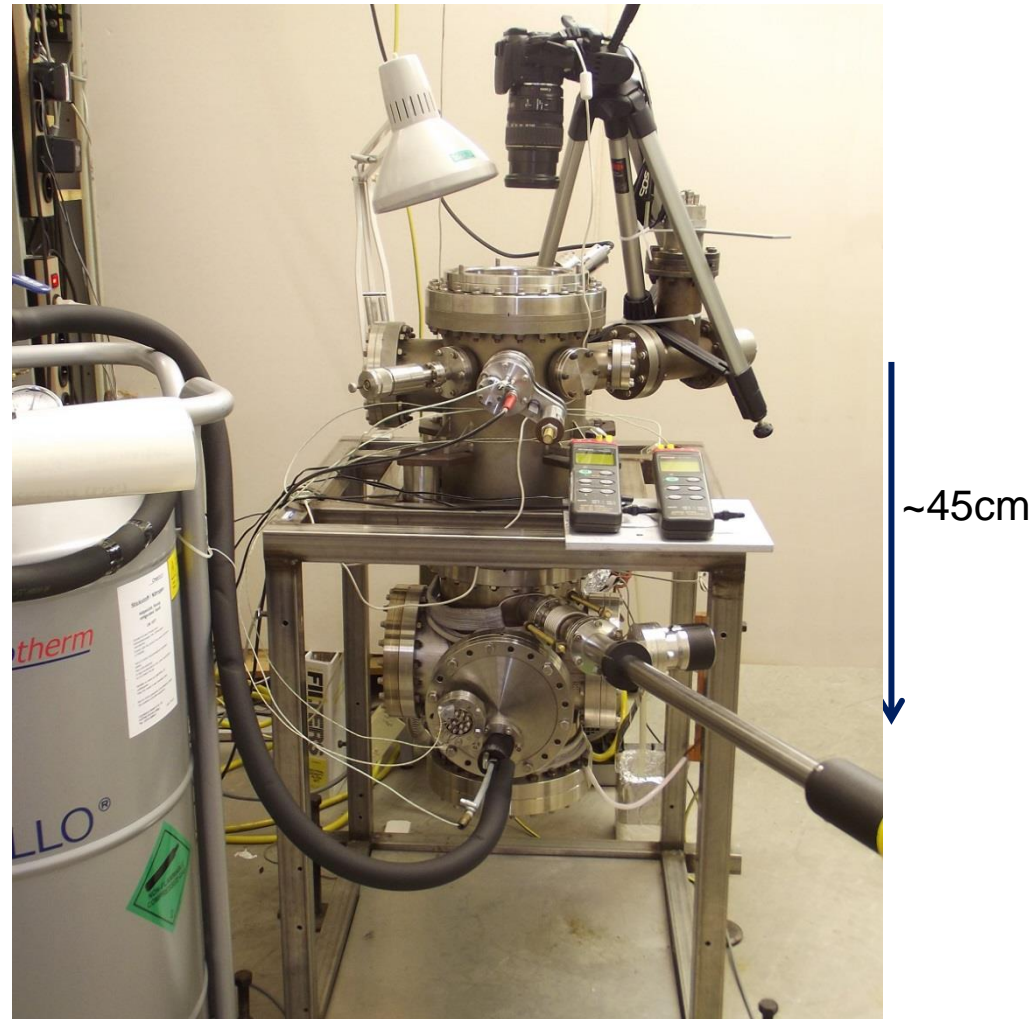
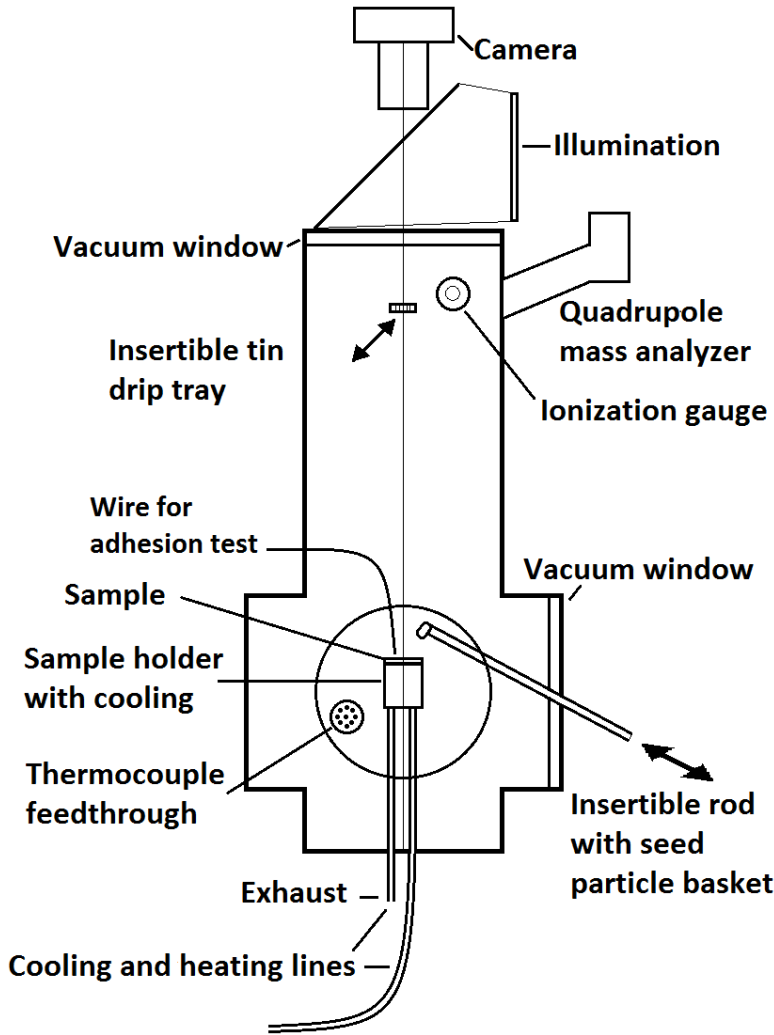
Cleaning

- Contamination of ML-coated mirror by large tin drops (99.999% purity)
- Seed initiation of phase transition at $-25\text{ }^{\circ}\text{C}$ to gray tin which breaks apart
- Subsequent surface cleaning by vibrations or flows of inert gas

First ex-situ tests: N. Böwering, Mater. Chem. Phys. **198**, 236 – 242 (2017)

Setup for In-Situ Tin Dripping in Vacuum

Can fit in MLM-samples and up to 6-inch wafers



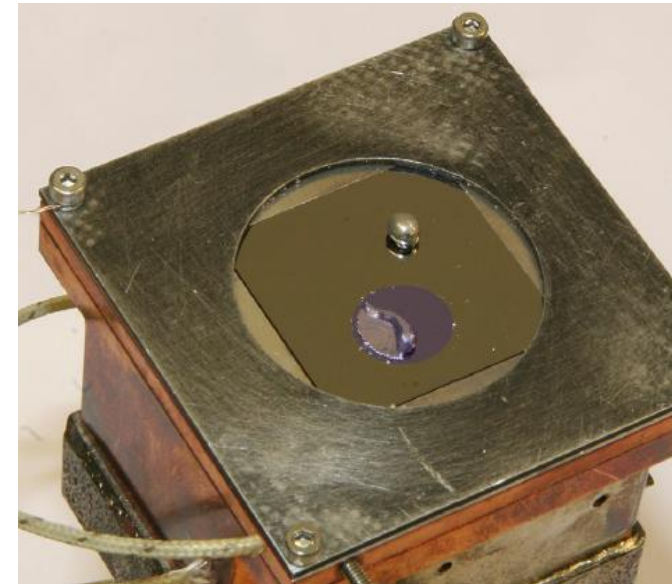
Sample cooling and heating capability; chamber base pressure: 10^{-7} mbar

Sticking Behavior of Tin Drops on Surfaces

Sticking depends on properties of substrate and coating:
Influence of material, substrate temperature and effusivity (heat conductance)

- Droplet splat **sticking** observed on heated smooth substrates, $T_s = \sim 90^\circ\text{C}$
- **Non-sticking** on Si substrates at room temperature or when cooled to -50°C
 Delamination behavior seen: droplet self-peeling or contraction dominates
 Bending force by surface tension of splat exceeds adhesion to substrate

Sample type/ T_s	$\sim 90^\circ\text{C}$	23°C	-50°C
Si wafer	Sticks	Peels	Peels
Si-ZrO ₂	Sticks	Peels, contracts	Contracts
Si-Mo/Si	Sticks	Peels	Contracts
Si-Mo/Si-ZrN	Sticks	Sticks or peels	Peels
Si-Mo/Si-ZrO ₂	Sticks	Sticks	Peels
Oxidized Si wafer	Sticks	Sticks	Peels
Glass slide	Sticks	Sticks	Sticks
Rough Si wafer	Peels	Peels, contracts	Contracts

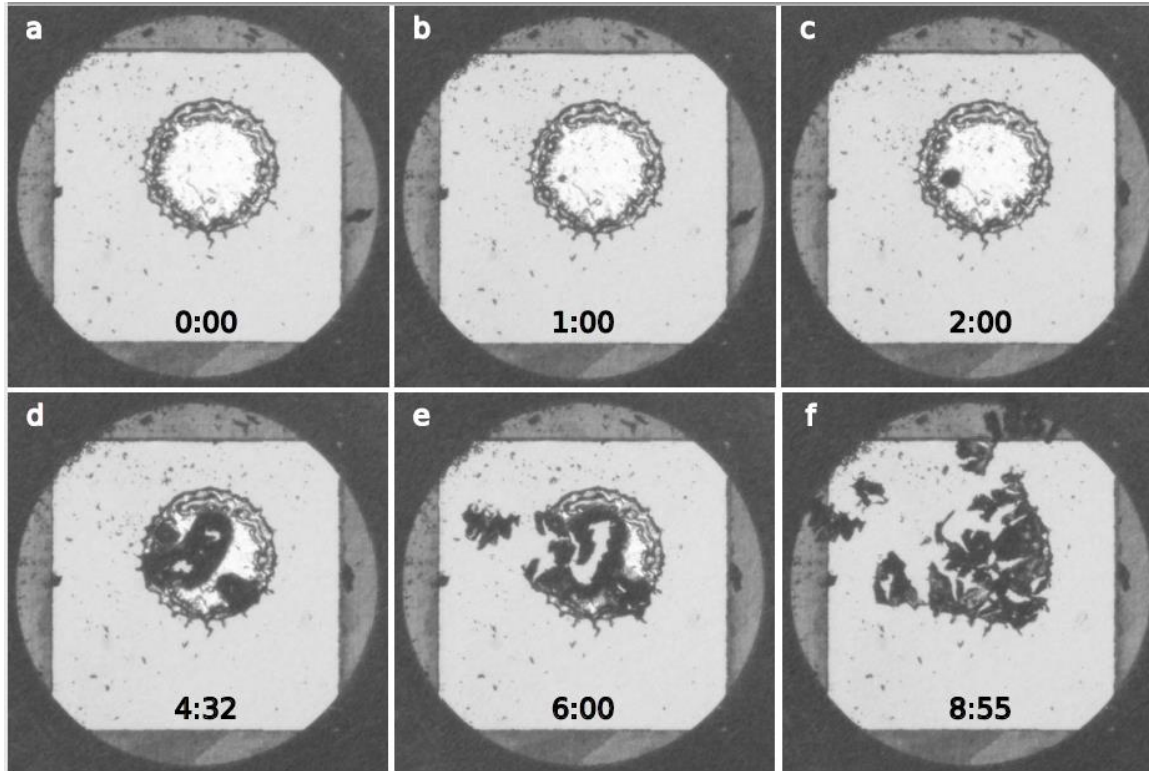


Fully and partially contracted splats

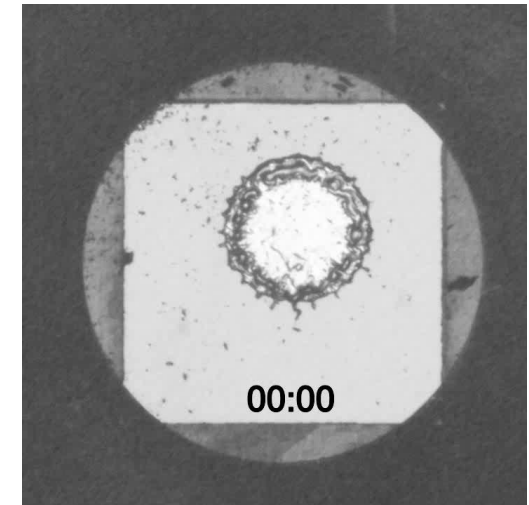
Sticking behavior: N. Böwering, C. Meier, Appl. Phys. A **125**, 633 (2019)

In-Situ Transformation of Tin Splat

Tin drop (154 mg) dripped on sample at $T_s = 92\text{ }^\circ\text{C}$. Growth of brittle gray tin: $v = 10\text{-}15\text{ }\mu\text{m}/\text{min}$. Substrate cooling at T_s of $-30\text{ }^\circ\text{C}$ to $-40\text{ }^\circ\text{C}$; ~ 9 hrs. to complete the transformation



$T_s \sim -35\text{ }^\circ\text{C}$



Time lapse video
(not included in pdf)

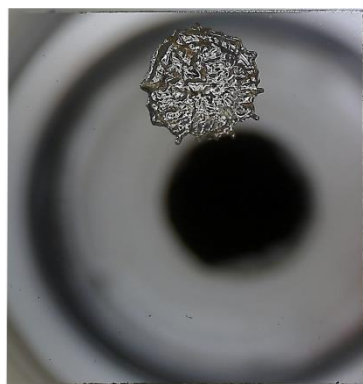
Coating of Si-sample: Mo/Si MLM with 3 nm thick ZrO_2 cap layer ($R_{\text{max}} = \sim 56\%$ at 13.5 nm)

Sticking behavior and transformation: N. Böwering, C. Meier, Appl. Phys. A **125**, 633 (2019)

Tin Drop Transformation on Multilayer-Coated Mirror Sample: EUV-Reflectance

EUV Reflectance at 13.6 nm for uncapped Mo/Si-coated sample:

Tin drop conversion during cooling in ~7 hours



after tin dripping

=>
T=-24°C



after conversion

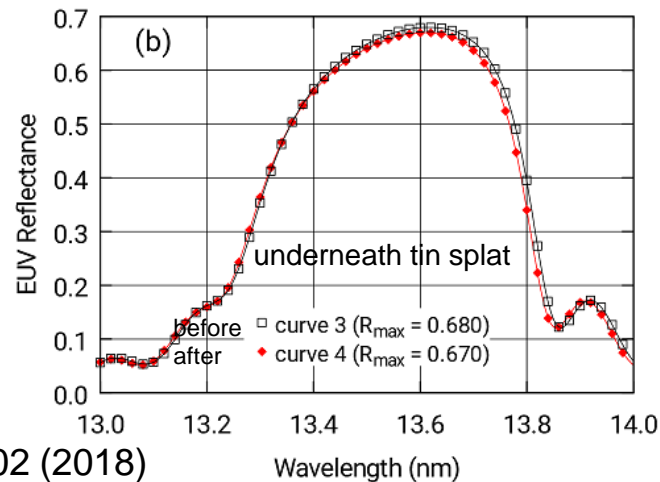
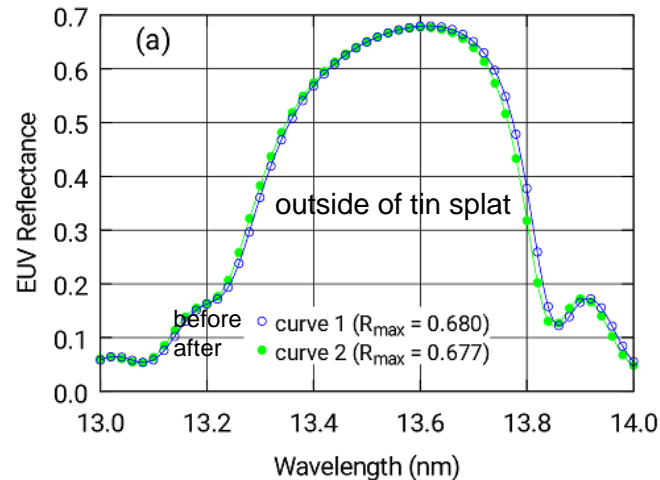
EUVR measurements by PTB:

Peak EUVR before tin dripping: $R_{\max} = 68.0\%$

Peak EUVR after tin cleaning: $R_{\max} \geq 67.0\%$

(a) R_{\max} : 67.2 % – 67.7 % outside of tin splat

(b) R_{\max} : 67.0 % underneath tin splat



EUVR results: N. Böwering, C. Meier, J. Vac. Sci. Technol. B **36**, 021602 (2018)

Tin Removal by CO₂ Snowflake Aerosol

Ex-situ removal by impact of CO₂ snow-flakes using a gun-jet nozzle with expansion of liquid carbon dioxide at high gas pressures

During expansion phase change of liquid CO₂ to small snow crystals with temperature of ~-70 °C

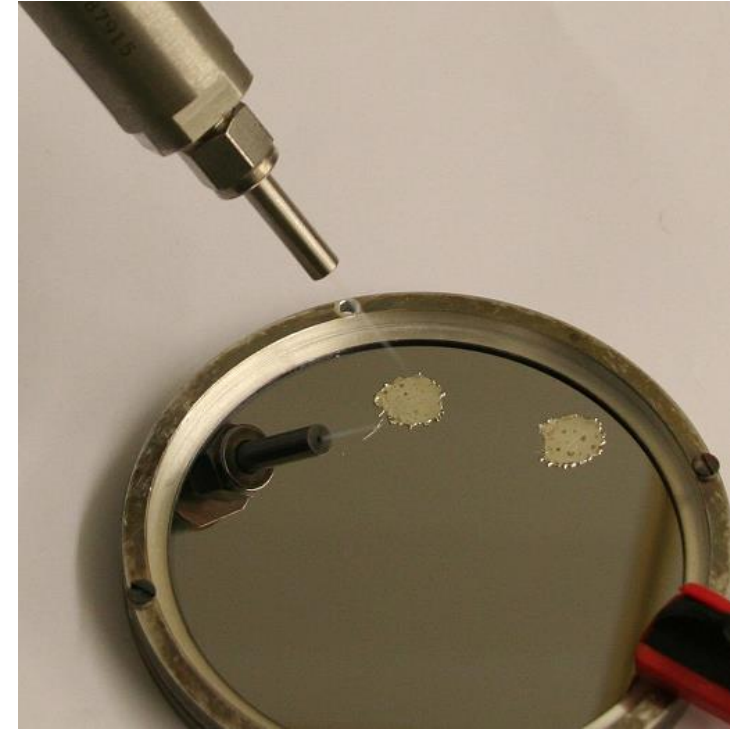
pressure: ~50 bar, filter nozzle: 1 mm diam.

Fast ex-situ removal technique with minute duration; works for thin and thick Sn deposits and also for other adhering contaminations

Process can be automated for repeated sweeping strokes across curved substrates

High-purity CO₂ gas should be used!

Organic residue seen when using industrial grade liquid CO₂ (99.5%)



Setup for CO₂ snow-jet cleaning of 4" Mo/Si-coated MLM wafer

EUV mask cleaning with CO₂ snow: Varghese et al., Proc. SPIE **8166**, 816615 (2011)

Alternative Cryogenic Sn-Removal Techniques

We have examined 5 different schemes at low temperatures

In-situ tin splat removal:

- Non-sticking at low substrate temperatures (*cooling to ~ -50 °C*)
- For sticking deposits:
 - Conversion to gray tin by tin pest (*phase transition, at $-25...-40$ °C*)
 - Delamination by strong cooling (*to ~ -120 °C, expansion difference*)

Ex-situ tin splat removal:

- Delamination after immersion in liquid nitrogen (*contraction difference, ~ -196 °C*)
- Removal by high-pressure CO₂ snow-flake aerosol (*cooling and impact, ~ -50 °C*)

Delamination due to thermal contraction mismatch:

CTE at 300 K of Si: $2.6 \cdot 10^{-6}/\text{K}$

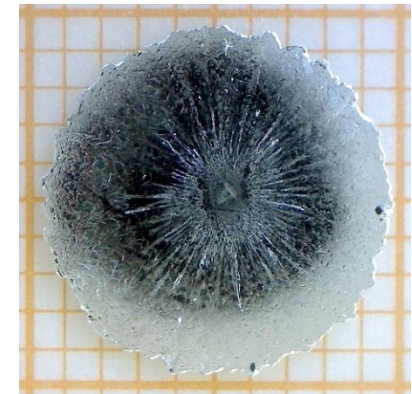
CTE at 300 K of β -Sn: $22 \cdot 10^{-6}/\text{K}$

No damage to ML coating seen

Compared to tin-etching by hydrogen radicals, all cryogenic techniques are faster by orders of magnitude!



Top of tin drop



Bottom of tin drop

6" Structured Si-Wafer Grating Sample

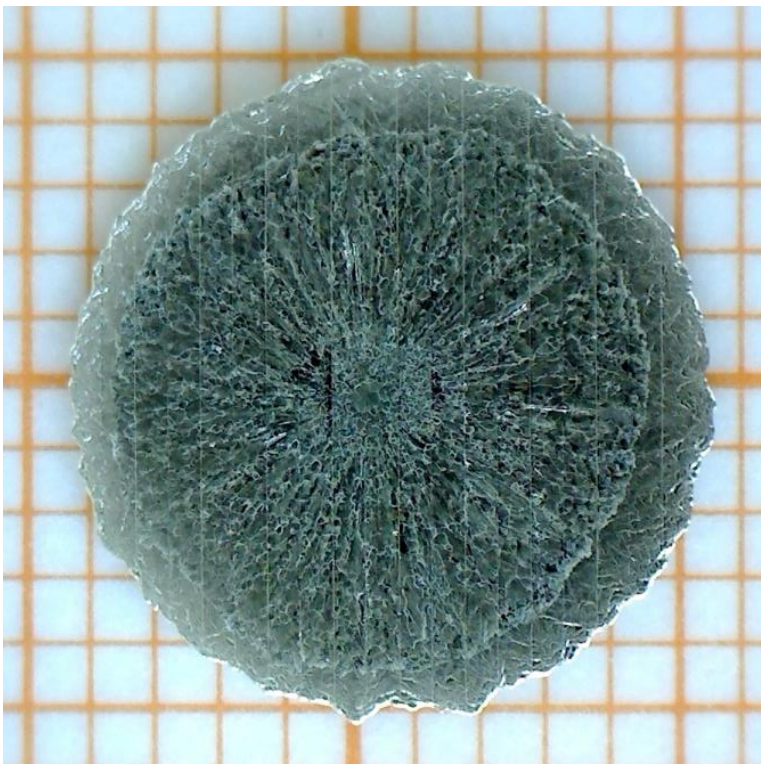
EUV collector mirrors use grating structures for suppression of IR radiation

M. Kriese et al., Proc. SPIE **9048**, 90483C (2014); T. Feigl et al., Proc. SPIE **9422**, 94220E (2015)

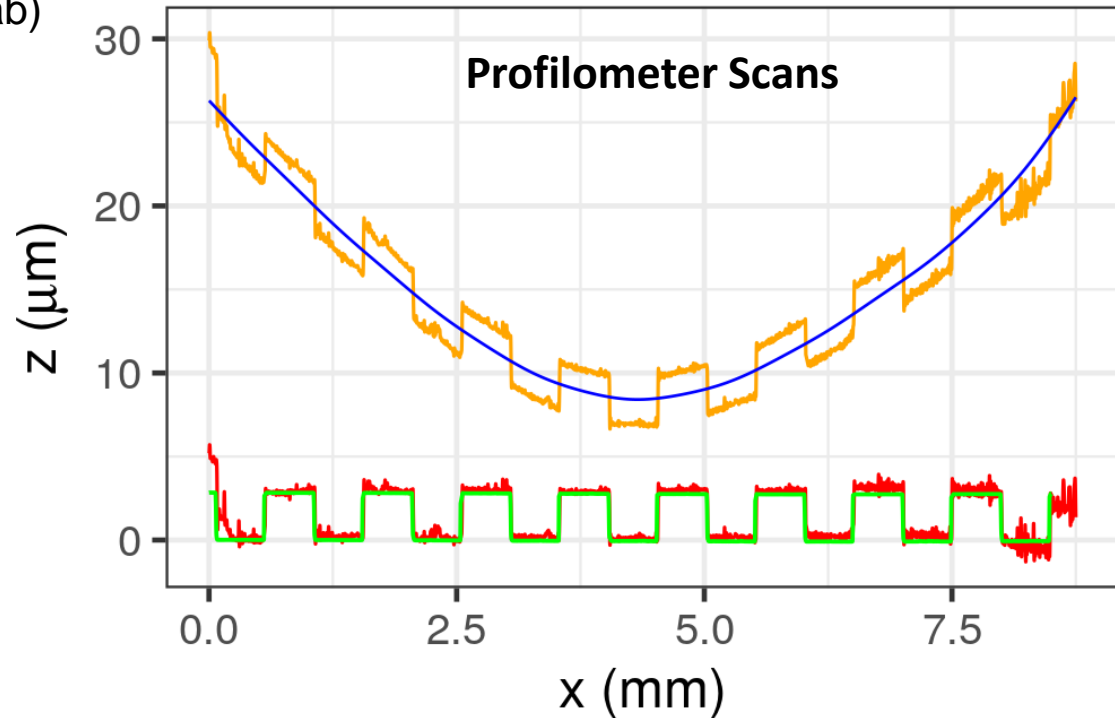
6" laminar grating on Si substrate

etched straight grooves (optiXfab)

0.5 mm wide, $\sim 3 \mu\text{m}$ deep



Grating structure imprinted on bottom of tin drop



- Bottom side of tin drop
- Spline fit to curvature
- Bottom side w/o curvature
- Scan of grating substrate

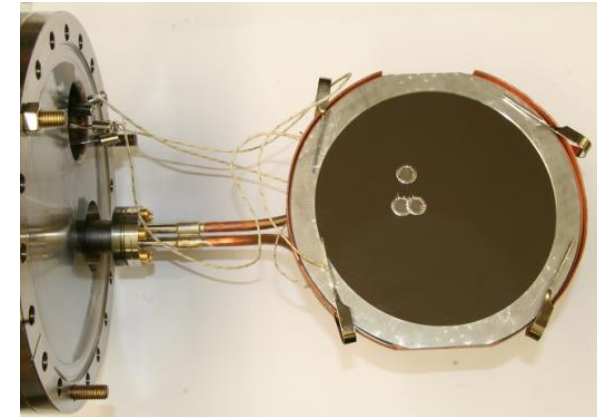
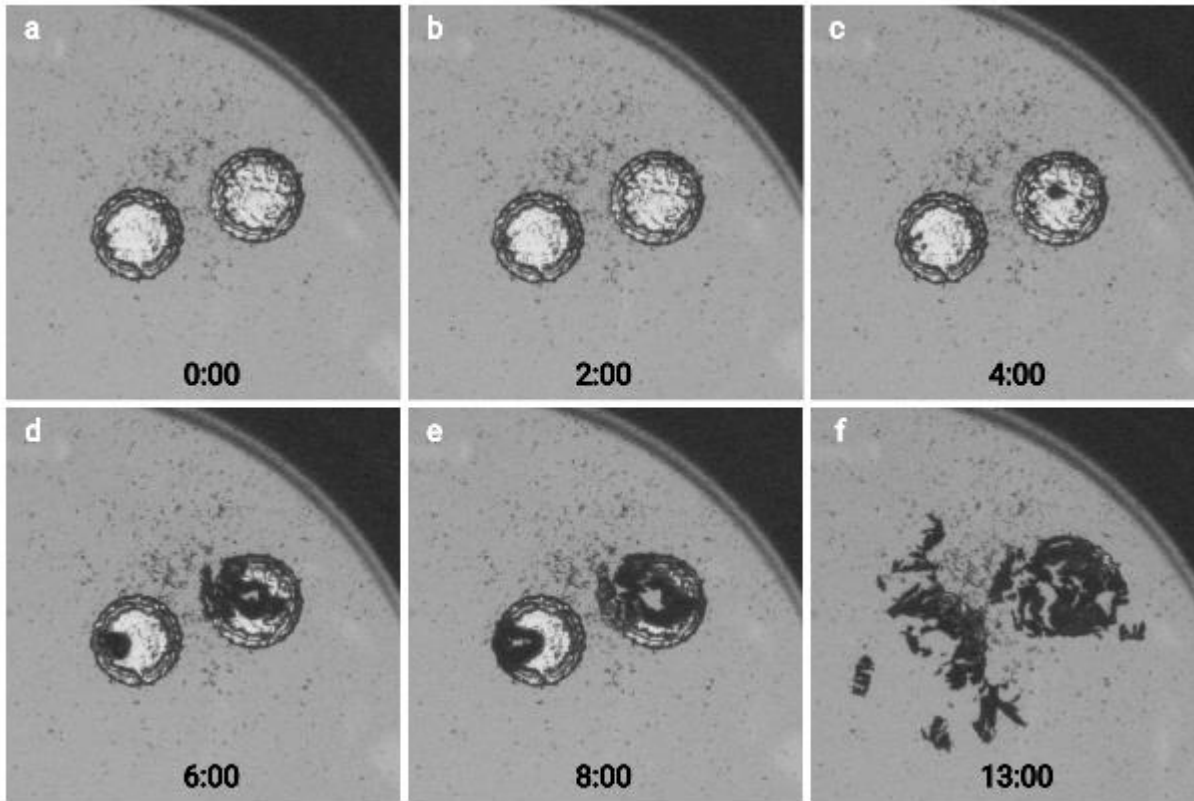
Drop removed from grating sample by cooling

In-situ Transformation on 6" Grating Sample

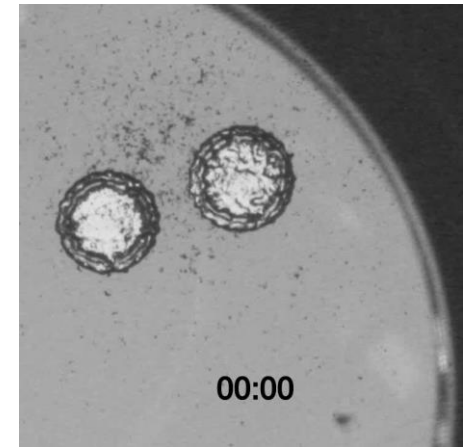
Similar phase transformation behavior observed on uncoated Si grating wafer*

* supplied by optiX.fab

$T_s \sim -40^\circ\text{C}$



Cooled sample holder



Time lapse video
(not included in pdf)

Droplet splat conversion to gray tin on uncoated Si grating wafer

“Gray tin on the grating”: N. Böwering, C. Meier, to be published

Summary: Cryogenic EUV Optics Tin-Cleaning

Prerequisite: Cooling to low temperatures of optics to be cleaned

Several simple, low-cost methods were tested successfully on different substrates:

- Non-sticking tin drops at/below room temperature on Si substrates
 - Induction of tin pest for sticking tin deposits on Si-MLM
 - Phase transformation applies specifically to tin contaminations
 - In-situ cleaning demonstrated inside of vacuum chamber
 - Fast cleaning of thick deposits by conversion in less than 24 hours
 - No damage of multilayer coating and grating
 - Reduction in EUVR is less than 0.5%
 - Alternatives: Delamination by cooling to very low temperatures ($< -100^{\circ}\text{C}$)
 - Ex-situ removal by impact of CO_2 snowflake jet
 - 5 different schemes examined on different substrates
- > EUV collectors should be cooled more strongly to mitigate tin contaminations*

Acknowledgements

- Thanks to optiXfab for providing ML-coated mirror and Si-wafer samples
- Thanks to PTB Berlin for a measurement of EUV reflectance

optiXfab.



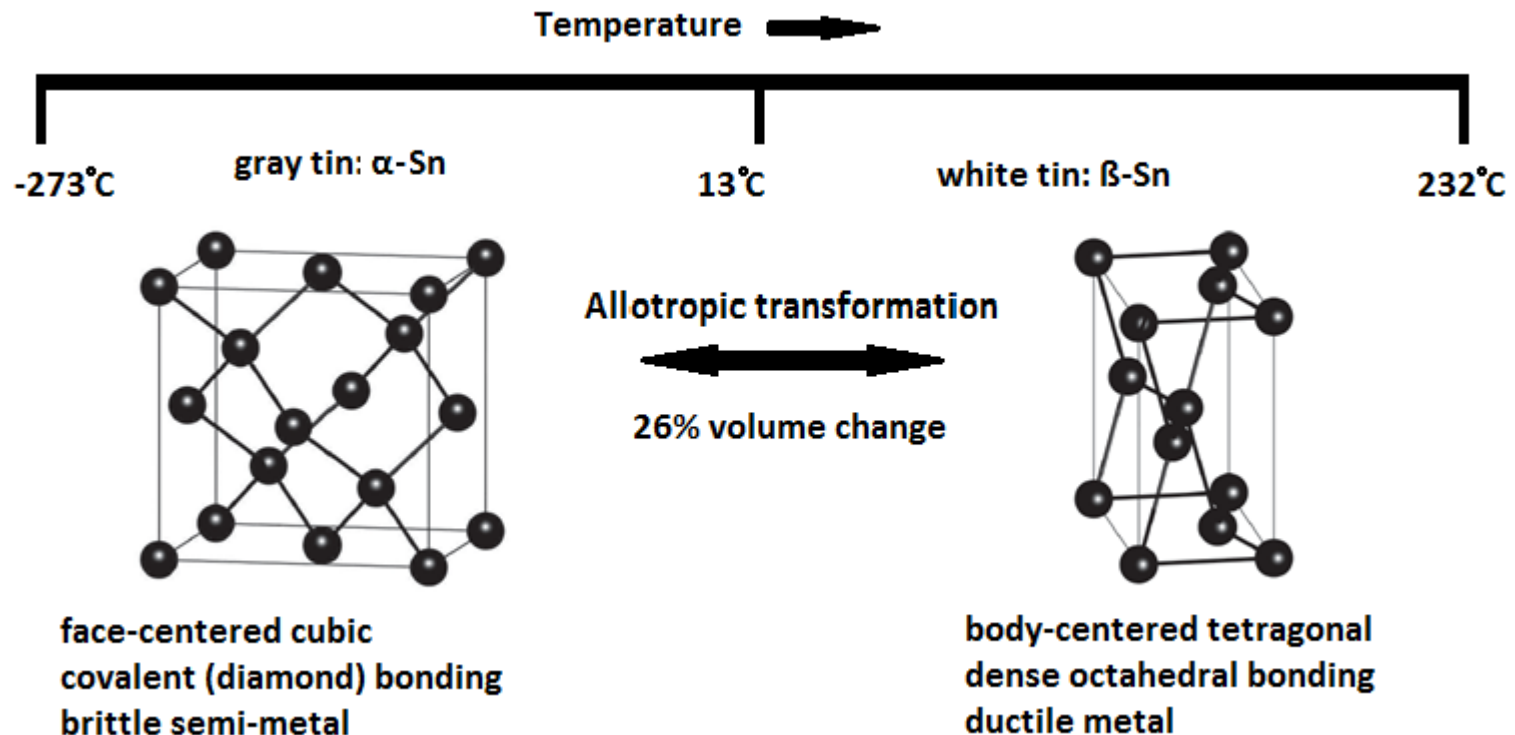
Thank you
for your attention!

May the source be with you!

*Research carried out without funding.
Any development funding welcome!*

Add'l. Slide: Transformation of Tin β -Sn \rightarrow α -Sn

- At -20°C to -50°C , white tin can undergo a phase transformation to brittle semi-metallic gray tin.
- The phase transition occurs only rarely, but it can be triggered by inoculation with seed particles.
- Tin breaks apart due to large volume increase and brittleness.



Add'l: Model for Splat Sticking or Detachment

Two semi-infinite bodies brought suddenly into contact,
hot tin drop splat and colder silicon substrate:



$$T_c = T_s + (T_d - T_s) (1 + e_s/e_d)^{-1} ; \text{ with } e = (k\rho c_p)^{1/2}$$

T_c : thermal contact temperature; T_s : substrate temperature; T_d : droplet temperature
 e_s : substrate effusivity; e_d : droplet effusivity; k : thermal conductivity; ρ : density; c_p : heat capacity

For Si and tin drops with $T_d = \sim 250$ °C, $T_s = 90$ °C, 23 °C, -50 °C:
Initial temperature at contact surface: $T_c = 138$ °C, 90 °C, 39 °C

for $T_c > \sim 100$ °C: adhesion strength > bending force: splat **sticks** at $T_s = \sim 90$ °C
for $T_c < \sim 100$ °C: adhesion strength < bending force: splat **peels** at $T_s = \sim -50$ °C

For splat detachment, the bending force during solidification has to overcome adhesion.